# Elastic wave propagation in periodic media with helical symmetry

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2 Accounting for continuous helical symmetry

3 Rotationally symmetric cross-sections

### Justifying the existence of wave modes in curved media

#### Wave modes in a curved direction s:

- $\propto e^{iks}$  with k: wavenumber along s $\frac{\partial(\cdot)}{\partial s} \xrightarrow{\text{Fourier transform}} +ik(\cdot)$
- separation of variables : the coefficients of equilibrium equations, including boundary conditions, must not depend on s (or must be Δ*l*-periodic)

Illustrative example: elasticity equilibrium equations in curvilinear coordinates

$$\sigma_{,j}^{ij} + \Gamma_{mj}^{i}\sigma^{mj} + \Gamma_{mj}^{j}\sigma^{im} + \rho\omega^{2}g^{ij}u_{j} = f^{i}, \text{avec}: \sigma^{ij} = C^{ijkl}\epsilon_{kl}, \epsilon_{kl} = \frac{1}{2}(u_{k,l} + u_{l,k} - \Gamma_{kl}^{m}u_{m})$$

 $\rightarrow$  the coefficients depend on the physical properties (here,  $\rho$  et  $C^{ijkl}$ ) but also on the Christoffel symbols  $\Gamma_{ii}^k$ , fonction of the metric tensor

#### Sufficient conditions for wave modes

- **Q** the cross-section does not vary with s (or is  $\Delta l$ -periodic)
- **Q** the physical properties remain constant with s (or are  $\Delta l$ -periodic)
- **(a)** the metric tensor,  $(\mathbf{g})_{ij} = \mathbf{g}_i \cdot \mathbf{g}_i$ , does not depend on s

where  $(\mathbf{g}_1, \mathbf{g}_2, \mathbf{g}_3) = (\frac{\partial \mathsf{OM}}{\partial x}, \frac{\partial \mathsf{OM}}{\partial y}, \frac{\partial \mathsf{OM}}{\partial s})$ : covariant basis of the curv. system (x, y, s)

### Some helical coordinate systems allowing a separation of variables

• Coordinate system about a single helix (x, y, s): OM(x, y, s) = R(s) + xN(s) + yB(s)with (x, y): coord. in a cross-section normal to the helix

$$\mathbf{g} = \begin{bmatrix} 1 & 0 & -\tau y \\ 0 & 1 & \tau x \\ -\tau y & \tau x & \tau^2 (x^2 + y^2) + (1 - \kappa x)^2 \end{bmatrix} = fct(x, y)$$





From a 3D structure to a 2D model (continuous sym. in s), and then to 2D/6 (discrete sym. in  $\theta$ )

### Some helical coordinate systems allowing a separation of variables

- Coordinate system about a single helix (x, y, s): OM(x, y, s) = R(s) + xN(s) + yB(s)with (x, y): coord. in a cross-section normal to the helix  $\mathbf{g} = \begin{bmatrix} 1 & 0 & -\tau y \\ 0 & 1 & \tau x \\ -\tau y & \tau x & \tau^2(x^2 + y^2) + (1 - \kappa x)^2 \end{bmatrix} = fct(x, y)$
- System of similar kind but polar  $(\rho, \theta, s)$ :  $OM(\rho, \theta, s) = R(s) + \rho \cos \theta N(s) + \rho \sin \theta B(s)$ with  $(\rho, \theta)$ : polar coord. in the cross-section

$$\mathbf{g} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \rho^2 & \tau^2 \rho^2 \\ 0 & \tau^2 \rho^2 & \tau^2 \rho^2 + (1 + \kappa \rho \cos \theta)^2 \end{bmatrix} = \mathsf{fct}(\rho) \text{ si } \kappa = 0$$





From a 3D structure to a 2D model (continuous sym. in s), and then to 2D/6 (discrete sym. in  $\theta$ )

- "Bi-helical" coordinate system  $(s_1, s_2, r)$ :
  - relation between cylindrical and helical coordinates:
    - $\begin{cases} \theta = \frac{2\pi}{l_1} s_1 + \frac{2\pi}{l_2} s_2 & L_{1,2} : \text{helix steps along } z \\ z = \frac{L_1}{l_1} s_1 + \frac{L_2}{l_2} s_2 & l_{1,2} : \text{steps measured along } s_{1,2} \end{cases}$
  - position vector  $\mathbf{OM}(s_1, s_2, r) = r\mathbf{e}_r(\theta) + z\mathbf{e}_z$

$$\mathbf{g} = \begin{bmatrix} \frac{4\pi^2 r^2 + L_1^2}{l_1^2} & \frac{4\pi^2 r^2 + L_1 L_2}{l_1 l_2} & 0\\ \frac{4\pi^2 r^2 + L_1 L_2}{l_1 l_2} & \frac{4\pi^2 r^2 + L_2^2}{l_2^2} & 0\\ 0 & 0 & 1 \end{bmatrix} = \mathsf{fct}(r)$$



A bi-helical periodic pattern  $(s_1, s_2)$ : helical coordinates



Example of bi-helical structure: chiral nanotube (discrete helical symmetry in  $s_1$  and  $s_2$ )

#### 2 Accounting for continuous helical symmetry

3 Rotationally symmetric cross-sections

Variational formulation for 3D elastodynamics:

$$\int_{\Omega} \delta \boldsymbol{\epsilon}^{\mathsf{T}} \mathbf{C} \boldsymbol{\epsilon} \mathrm{d} \boldsymbol{V} + \int_{\Omega} \rho \delta \mathbf{u}^{\mathsf{T}} \ddot{\mathbf{u}} \mathrm{d} \boldsymbol{V} = \mathbf{0}, \text{ with } \boldsymbol{\epsilon} = (\mathbf{L}_{xy} + \mathbf{L}_{z} \partial / \partial z) \mathbf{u}$$

Perform:

**•** Fourier transform along t and z:

$$\hat{\mathbf{u}}(k,\omega) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \mathbf{u}(z,t) \mathrm{e}^{-\mathrm{i}(kz-\omega t)} \mathrm{d}z \mathrm{d}t$$

**Q** FE discretization of the cross-section (x, y):

$$\Rightarrow \mathbf{u}(x, y, z, t) = \mathbf{N}^{e}(x, y)\mathbf{U}^{e}e^{\mathbf{i}(kz-\omega t)}$$

#### Quadratic eigenvalue problem

$$[\mathbf{K}_1 - \omega^2 \mathbf{M} + \mathrm{i}k(\mathbf{K}_2 - \mathbf{K}_2^T) + k^2 \mathbf{K}_3]\mathbf{U} = \mathbf{0}$$

- problem reduced on the cross-section only
- solved for each frequency  $\omega$ , solution = guided modes  $(k_n^{\pm}, \mathbf{U}_n^{\pm})$



3D waveguide of arbitrary cross-section



SAFE mesh

### Accounting for continuous helical symmetry

- Strain tensor (covariant components):  $\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}) \Gamma_{ij}^k u_k$
- Transformation into the orthonormal basis (N, B, T) (\*):  $\epsilon_{ij} \longrightarrow \epsilon_{\alpha\beta} (\alpha, \beta = n, b, t)$ (\*) more convenient because the helical covariant and contravariant bases are not orthogonal

#### $\Rightarrow$ Strain in Serret-Frenet basis:

$$\boldsymbol{\epsilon} = (\mathbf{L}_{xy} + \mathbf{L}_{s}\partial/\partial s)\mathbf{u} \quad \text{with: } \mathbf{u} = [u_{n} \ u_{b} \ u_{t}]^{T}, \ \boldsymbol{\epsilon} = [\epsilon_{nn} \ \epsilon_{bb} \ \epsilon_{tt} \ 2\epsilon_{nb} \ 2\epsilon_{nt} \ 2\epsilon_{bt}]^{T}$$
$$\mathbf{L}_{xy} = \frac{1}{1+\kappa x} \begin{bmatrix} (1+\kappa x)\partial/\partial x & 0 & 0\\ 0 & (1+\kappa x)\partial/\partial y & 0\\ \kappa & 0 & \tau y\partial/\partial x - \tau x\partial/\partial y\\ (1+\kappa x)\partial/\partial y & (1+\kappa x)\partial/\partial x & 0\\ \tau y\partial/\partial x - \tau x\partial/\partial y & -\tau & -\kappa + (1+\kappa x)\partial/\partial x\\ \tau & \tau y\partial/\partial x - \tau x\partial/\partial y & (1+\kappa x)\partial/\partial y \end{bmatrix}$$
$$\mathbf{L}_{s} = \frac{1}{1+\kappa x} \begin{bmatrix} 0 & 0 & 0\\ 0 & 0 & 0\\ 0 & 0 & 0\\ 1 & 0 & 0\\ 0 & 1 & 0 \end{bmatrix}$$

What is the appropriate coordinate system for helical symmetry ?



The seven-wire strand case

- central wire: Cartesian system  $(\kappa, \tau) = (0, 0)$
- peripheral wires: helical systems with the same  $(\kappa, \tau)$  BUT different helix centrelines...
- seven-wire strand: TWISTING system ( $\kappa = 0, \tau = 2\pi/L \neq 0$ )





- $\bigcirc$  cross-section √
- **Q** physical properties  $\checkmark$
- 🧿 metric tensor √

Accounting for continuous helical symmetry

#### 3 Rotationally symmetric cross-sections

### Rotationally symmetric cross-sections

**Rotational symmetry**: non-translational, once again ( $\kappa \neq 0, \tau = 0$ )... but now the symmetry is of **discrete** type  $\Rightarrow$  circular periodicity



• Reminder: Bloch-Floquet boundary conditions (see e.g. Mead JSV 1996)



 $\mathbf{U}_r = \lambda \mathbf{U}_l, \quad \mathbf{F}_r = -\lambda \mathbf{F}_l$  $\lambda = e^{i\mu}$  (i $\mu$ : propagation constant)

straight periodicity, unit cell

• In case of circular periodicity:  $\lambda^N = 1$  (*N*: order of rotational symmetry)



circular periodicity with N cells

$$\lambda(n) = e^{i2n\pi/N}$$

$$n = \begin{cases} -\frac{N}{2} + 1, ..., 0, ..., \frac{N}{2} & \text{for } n \text{ even} \\ -\frac{N-1}{2}, ..., 0, ..., \frac{N-1}{2} & \text{for } n \text{ odd} \end{cases}$$

## Accounting for rotational symmetry in SAFE

Partition of dofs in SAFE:

$$\{\mathbf{K}_1 - \omega^2 \mathbf{M} + ik(\mathbf{K}_2 - \mathbf{K}_2^{\mathsf{T}}) + k^2 \mathbf{K}_3\} \mathbf{U} = \mathbf{F}$$
$$\mathbf{U} = [\mathbf{U}_I^{\mathsf{T}} \mathbf{U}_i^{\mathsf{T}} \mathbf{U}_r^{\mathsf{T}}]^{\mathsf{T}} \text{ and } \mathbf{F} = [\mathbf{F}_I^{\mathsf{T}} \mathbf{F}_i^{\mathsf{T}} \mathbf{F}_r^{\mathsf{T}}]^{\mathsf{T}}$$



**Q** Elasticity variables = **U** and **F**  $\rightarrow$  vectorial fields written in the (x, y, s) frame!

$$\mathbf{Q}_r \mathbf{U}_r = \lambda \mathbf{Q}_l \mathbf{U}_l \tag{2a}$$

$$\mathbf{Q}_r \mathbf{F}_r = -\lambda \mathbf{Q}_l \mathbf{F}_l \tag{2b}$$

**Q**<sub>1,r</sub>: transformation of vector components (x,y) to polar  $(r,\theta)$ **O** Build the projection matrix **R** from Eq. (2a):

$$\mathbf{U} = \mathbf{R}(n)\tilde{\mathbf{U}}, \quad \mathbf{R}(n) = \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{I} \\ \lambda(n)\mathbf{Q}_r^{-1}\mathbf{Q}_l & \mathbf{0} \end{bmatrix}, \quad \tilde{\mathbf{U}} = \begin{bmatrix} \mathbf{U}_l \\ \mathbf{U}_l \end{bmatrix}.$$

Trick: left multiply SAFE by R\*

$$\begin{bmatrix} \tilde{\mathbf{K}}_{1}(n) - \omega^{2} \tilde{\mathbf{M}}(n) + ik(\tilde{\mathbf{K}}_{2}(n) - \tilde{\mathbf{K}}_{2}(-n)^{\mathsf{T}}) + k^{2} \tilde{\mathbf{K}}_{3}(n) \end{bmatrix} \tilde{\mathbf{U}} = \mathbf{R}(n)^{*} \mathbf{F} = \mathbf{0} \text{ with } (\tilde{\mathbf{\cdot}}) = \mathbf{R}^{*}(\mathbf{\cdot}) \mathbf{R}$$
  
notice that  $\mathbf{R}(n)^{*} \mathbf{F} = \begin{bmatrix} \mathbf{F}_{l} + \lambda(n)^{*} \mathbf{Q}_{l}^{-1} \mathbf{Q}_{r} \mathbf{F}_{r} \\ \mathbf{0} \end{bmatrix} = \mathbf{0} \text{ from Eq. (2b)}$ 

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### WFEM: accounting for discrete helical symmetry in two directions

FE discretization of the unit cell:

$$(\mathbf{K} - \omega^2 \mathbf{M} - \mathrm{i}\omega \mathbf{C})\mathbf{U} = \mathbf{F}$$

#### Apply:

Displacement boundary conditions of Floquet-Bloch type (two-directional):

$$\begin{split} \mathbf{J}_{R}^{\mathsf{T}}\mathbf{U}_{R} &= \lambda_{1}\mathbf{J}_{L}^{\mathsf{T}}\mathbf{U}_{L}, \quad \mathbf{J}_{T}^{\mathsf{T}}\mathbf{U}_{T} = \lambda_{2}\mathbf{J}_{B}^{\mathsf{T}}\mathbf{U}_{B}, \quad \mathbf{J}_{RB}^{\mathsf{T}}\mathbf{U}_{RB} = \lambda_{1}\mathbf{J}_{LB}^{\mathsf{T}}\mathbf{U}_{LB} \\ \mathbf{J}_{LT}^{\mathsf{T}}\mathbf{U}_{LT} &= \lambda_{2}\mathbf{J}_{LB}^{\mathsf{T}}\mathbf{U}_{LB}, \quad \mathbf{J}_{RT}^{\mathsf{T}}\mathbf{U}_{RT} = \lambda_{1}\lambda_{2}\mathbf{J}_{LB}^{\mathsf{T}}\mathbf{U}_{LB} \end{split}$$

with:  $\lambda_1 = e^{ik_1\Delta l_1}$ ,  $\lambda_2 = e^{ik_2\Delta l_2}$  ( $k_1$ ,  $k_2$ : helical wavenumbers)

Force boundary conditions (by condensation of displacement)

<u>Remark 1</u>: displacement = vector  $\rightarrow$  must be in the covariant basis

$$\begin{bmatrix} \mathbf{g}_1 \\ \mathbf{g}_2 \\ \mathbf{g}_3 \end{bmatrix} = \mathbb{J}^{\mathsf{T}} \begin{bmatrix} \mathbf{e}_x \\ \mathbf{e}_y \\ \mathbf{e}_z \end{bmatrix}, \quad \mathbf{J}^{\mathsf{T}} = \begin{bmatrix} -\frac{2\pi r}{h}\sin\theta & \frac{2\pi r}{h}\cos\theta & \frac{L_1}{h} \\ -\frac{2\pi r}{h}\sin\theta & \frac{2\pi r}{h}\cos\theta & \frac{L_2}{h} \\ \cos\theta & \sin\theta & 0 \end{bmatrix}$$

<u>Remark 2</u>: the unit cell is delimited by non-plane surfaces (helicoids) <u>Remark 3</u>:  $k_1$  and  $k_2$  are not independent on eachother  $(\lambda_1^{N_2} \lambda_2^{-N_1} = 1)$ 



Unit cell example (a thick tube)

