

Fabrication additive & besoins en CND

Institut de Recherche en Génie Civil et Mécanique,
Equipe Etat Mécanique et Microstructure des Matériaux (E3M)

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La fabrication additive : principe - intérêt

Présentation de différents procédés

Réaliser un cordon

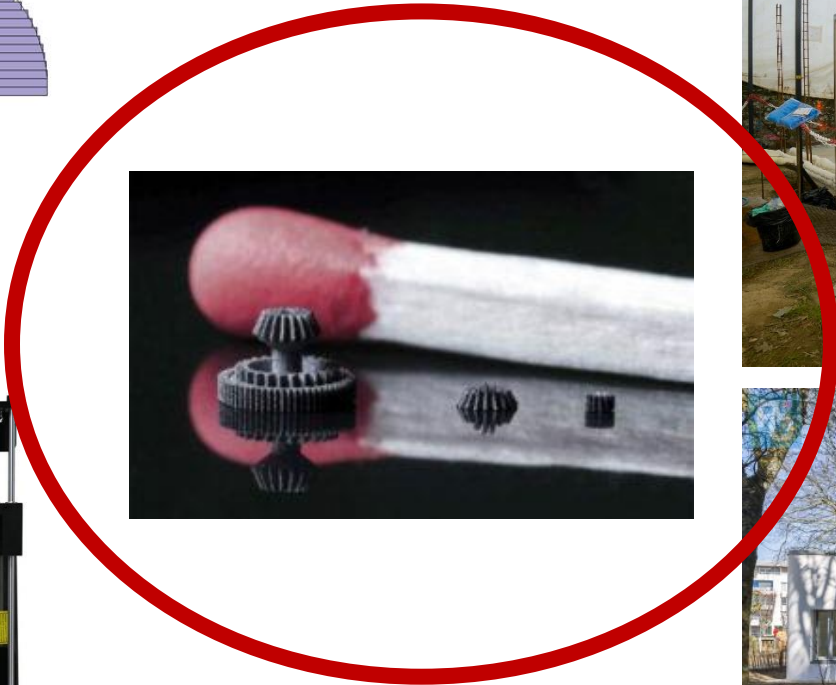
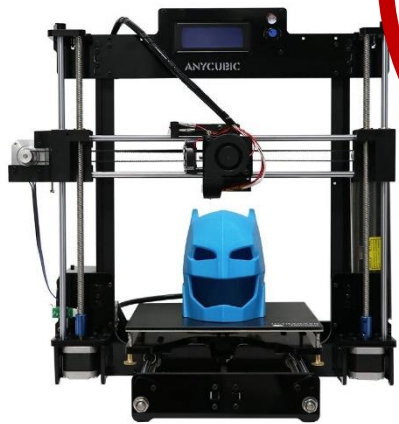
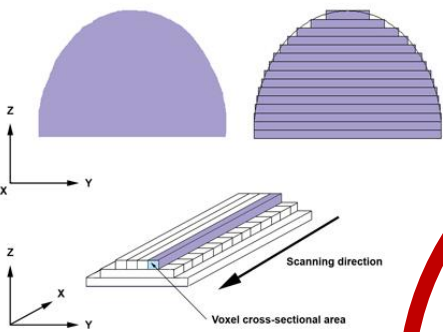
Réaliser un mur

Réaliser une structure pleine

Réaliser une pièce

Conclusion

Principe



Avantages

Plus rapide

Pas d'outil
Pas de moule

Plus souple

Géométrie complexe
Multi-matériaux
Plus esthétique
Personnalisation

Plus écologique

Pas d'enlèvement de matière
Moins de matière
Moins de transport

Plus économique

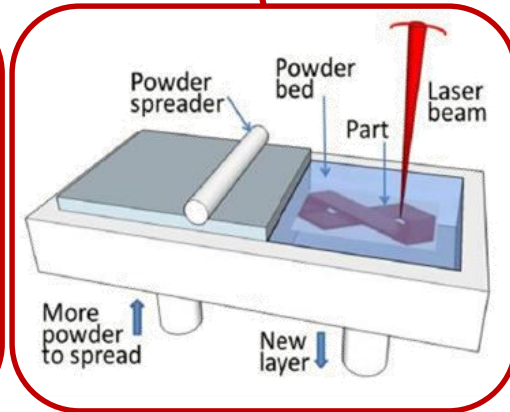
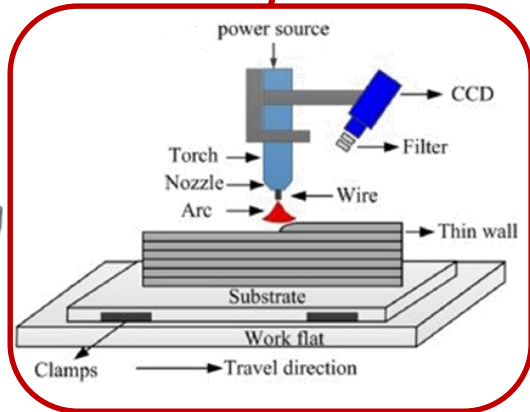
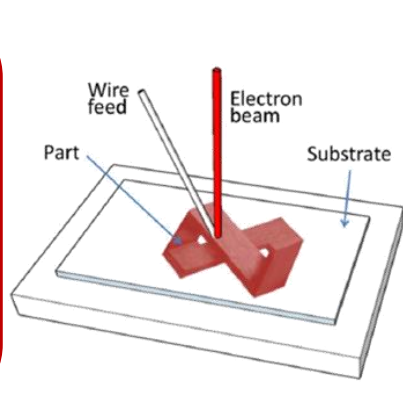
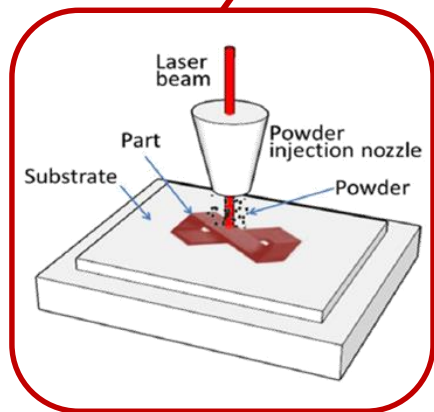
Pour toutes ces raisons

Inconvénients :

- Nécessité d'un post-traitement
- Nuances limitées de matériaux
- Limitation aux petites séries

Les procédés de fabrication additive avec fusion (matériaux métalliques)

Procédé	Dépôt de matériaux et fusion			Fusion sur lit de poudre	
	Poudre	Fil	Fil	Poudre	Faisceau d'électrons
Forme d'apport	Poudre	Fil	Fil	Poudre	Faisceau d'électrons
Source d'énergie	Laser	Faisceau d'électrons	Arc électrique	Laser	Faisceau d'électrons
Puissance (W)	100-3000	500-2000	1000-3000	50-1000	50-1000
Vitesse de dépôt (g/s)	0,1-1	0,1-2	0,2-2,8	-	-
Taille maximale de construction (mm x mm x mm)	2000x1500x750	2000x1500x750	5000x3000x1000	500x280x320	500x280x320
Précision dimensionnelle (mm)	0,5-1	1-1,5	Géométries trop complexes inaténables	0,04-0,2	0,04-0,2
Rugosité (µm)	4-10	8-15	Necessite un usinage de finition	7-20	7-20
Post process	CIC et usinage de finition	Usinage de finition	Ré-usinage et usinage de finition	CIC parfois recommandé	CIC parfois recommandé

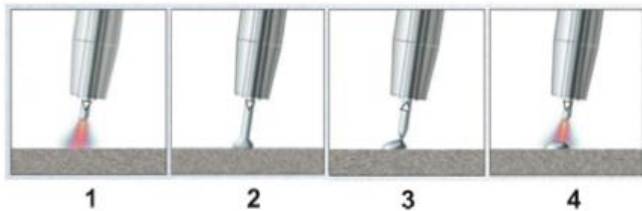


+ projection à froid (Coldspray)

Fabrication Additive Arc Fil : MIG-CMT

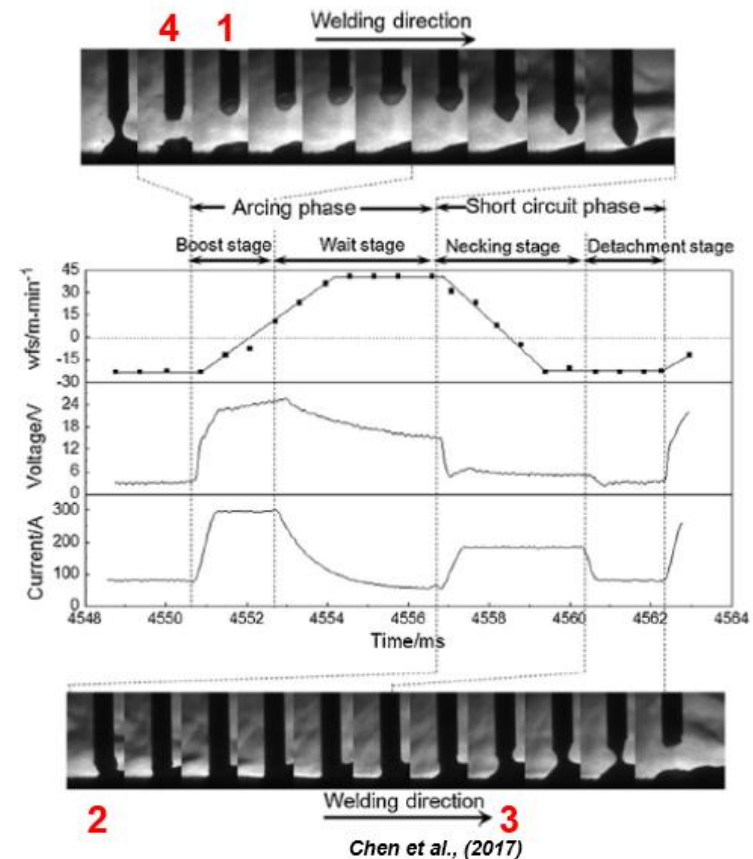
Metal Inert Gas – Cold Metal Transfert

- Procédé contrôlé
- Mode de transfert peu énergétique
- Couplage d'une impulsion électrique + mécanique

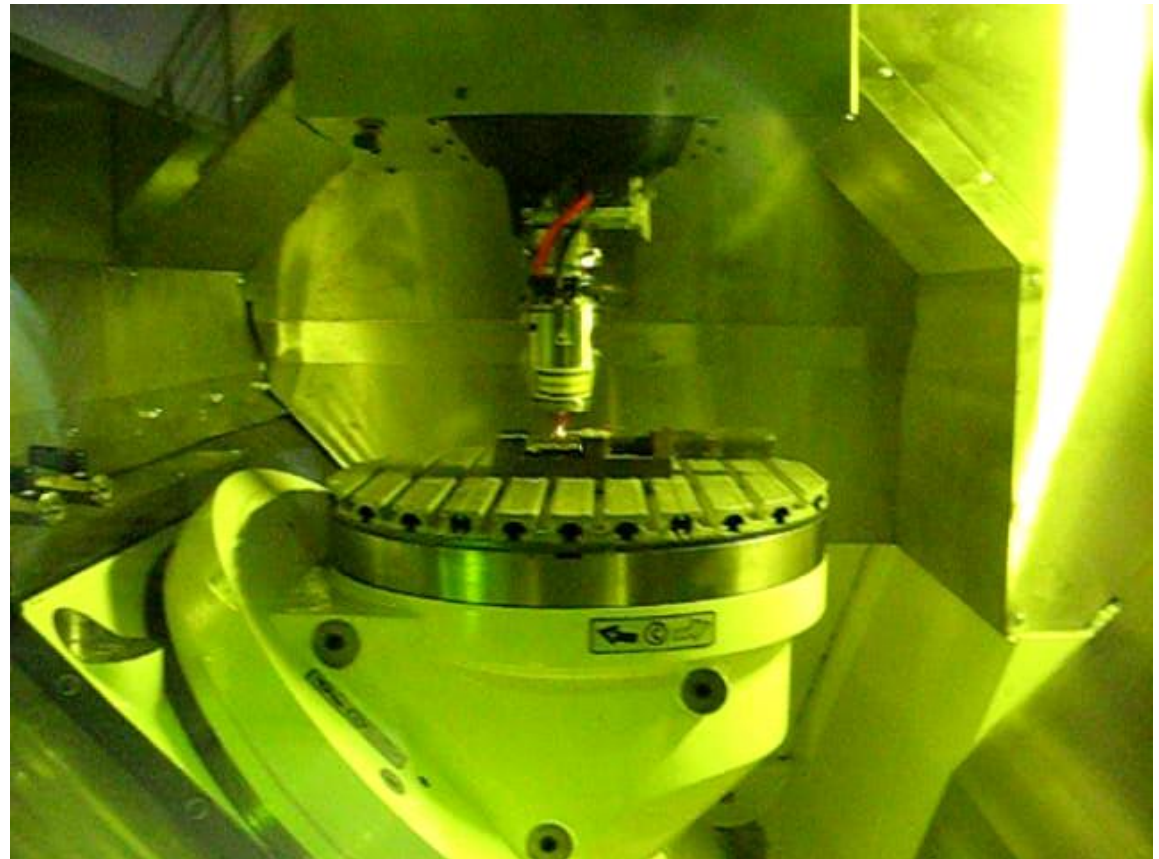
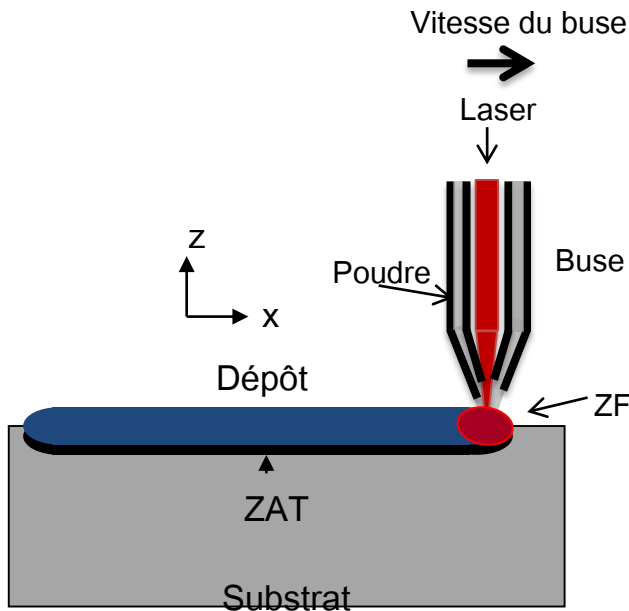
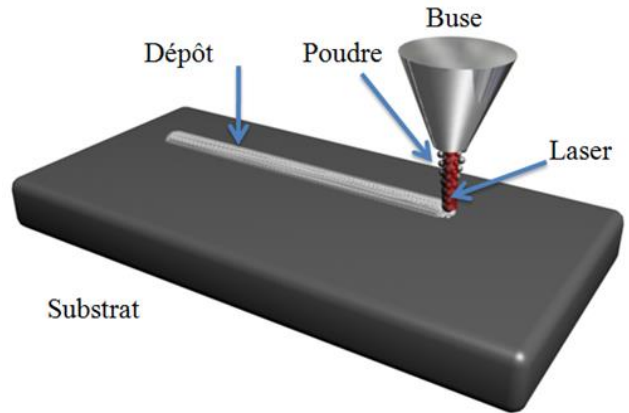


- 1 - Approche fil + l'arc s'établit + création d'une goutte
- 2 - Le fil apporte la goutte dans le bain de fusion + CC : poste $I \approx 0$
- 3 - Le fil se rétracte et détache la goutte
- 4 - Le fil ressort et le cycle redémarre

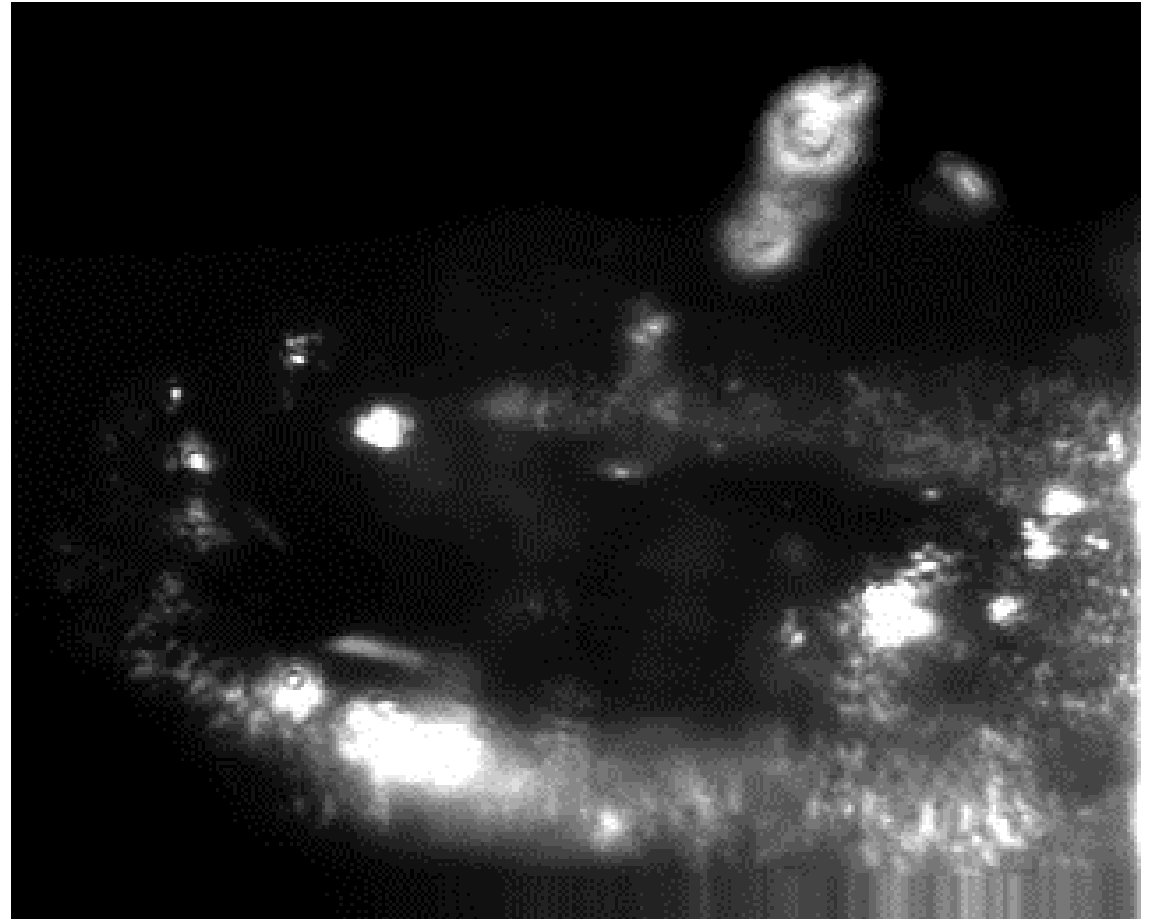
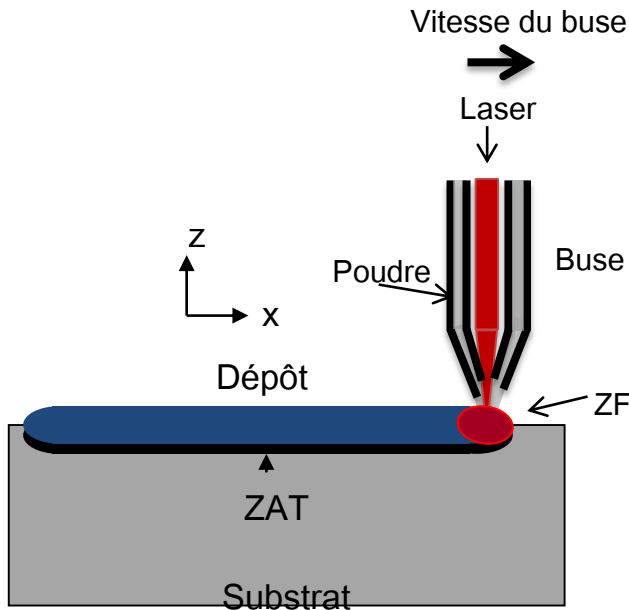
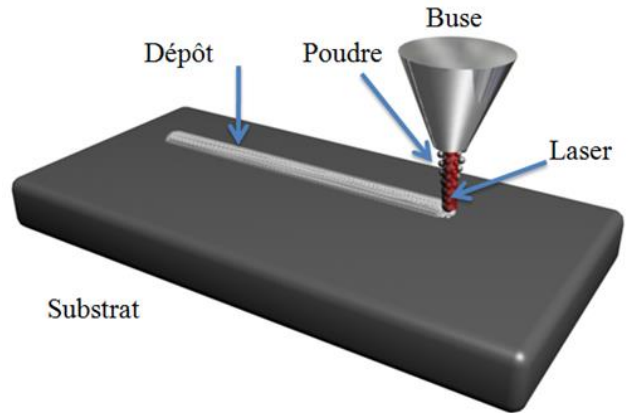
Fronius, (2011)



Direct Metal Laser Deposition : projection de la poudre dans le faisceau laser



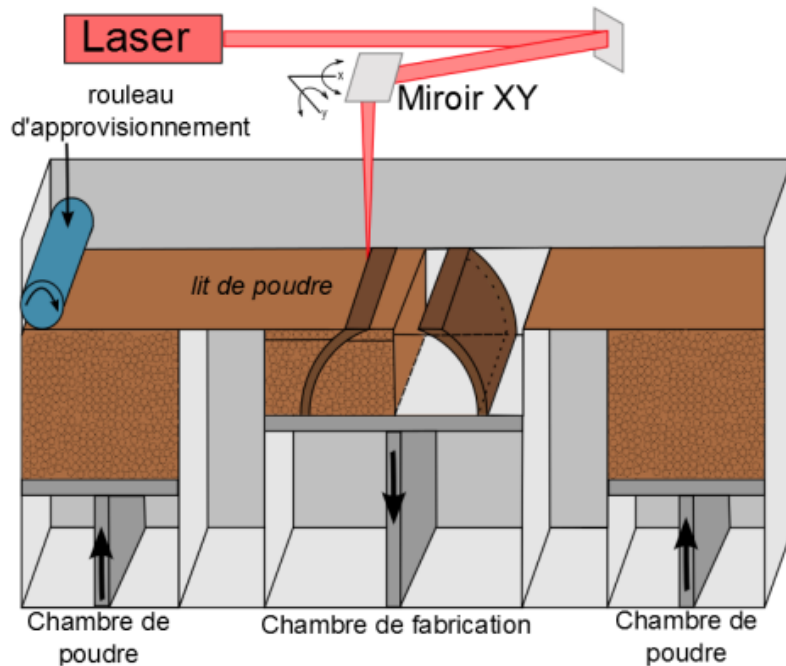
Direct Metal Laser Deposition : projection de la poudre dans le faisceau laser



Observations of Particle-Melt Pool Impact Events DLMD

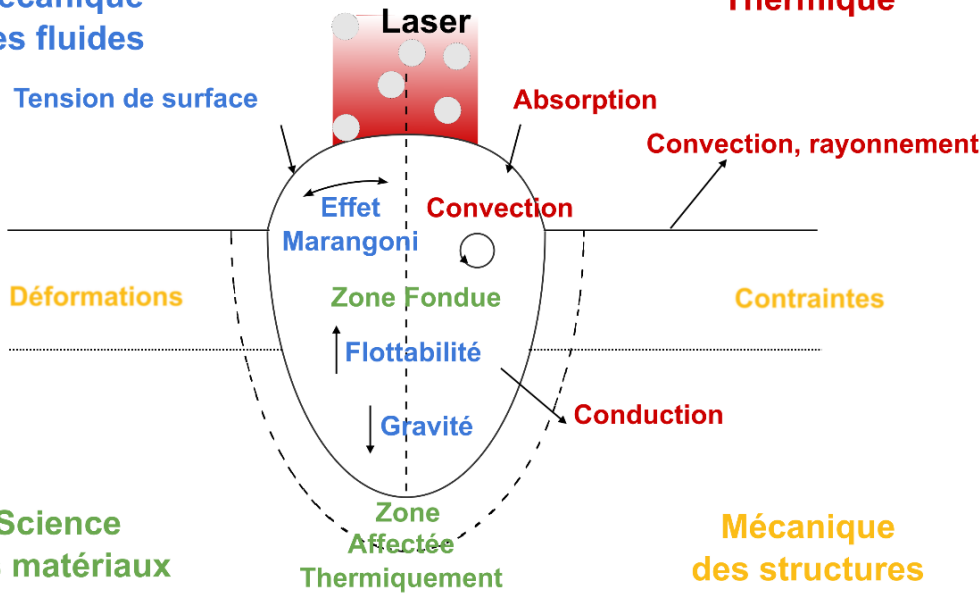
Additive Manufacturing 22 (2018) 368–374

Selective Laser Melting : Le faisceau laser provoque la fusion d'une couche de poudre pré-déposée



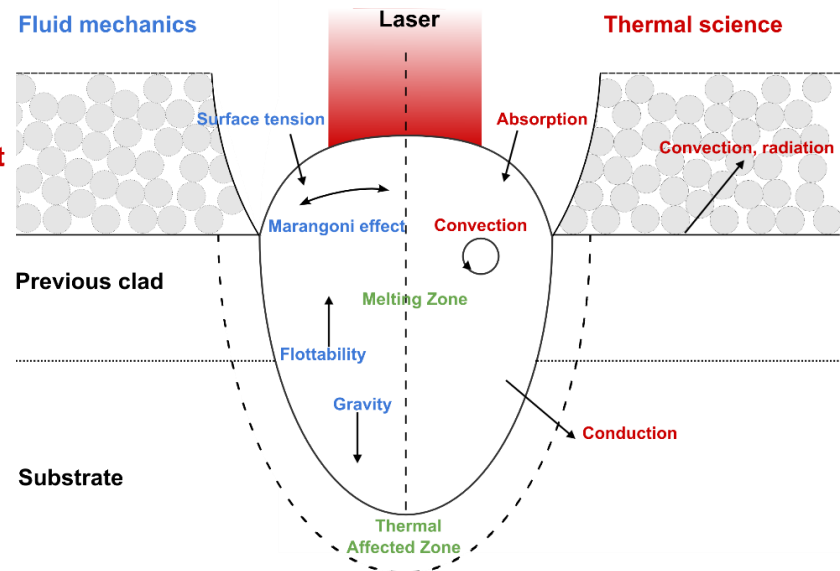
Mécanique des fluides

Thermique



Fluid mechanics

Thermal science



Réaliser un cordon

Non fusion d'une partie de la poudre

Materials and Design 95 (2016) 431–445

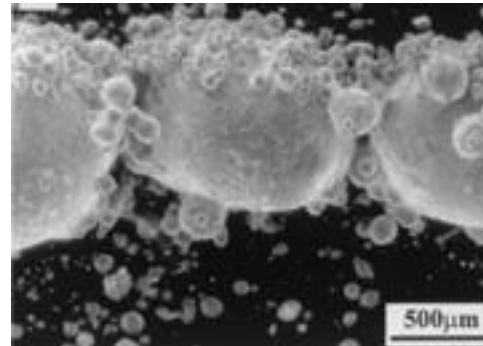


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Materials and Design

journal homepage: www.elsevier.com/locate/matdes

Review of in-situ process monitoring and in-situ metrology for metal additive manufacturing

Sarah K. Everton ^{a,b,*}, Matthias Hirsch ^a, Petros Stravroulakis ^a, Richard K. Leach ^a, Adam T. Clare ^a^a Department of Mechanical, Materials and Manufacturing Engineering, University of Nottingham, University Park, Nottingham NG72RD, United Kingdom^b Manufacturing Technology Centre, Ansty Park, Coventry CV7 9JU, United Kingdom

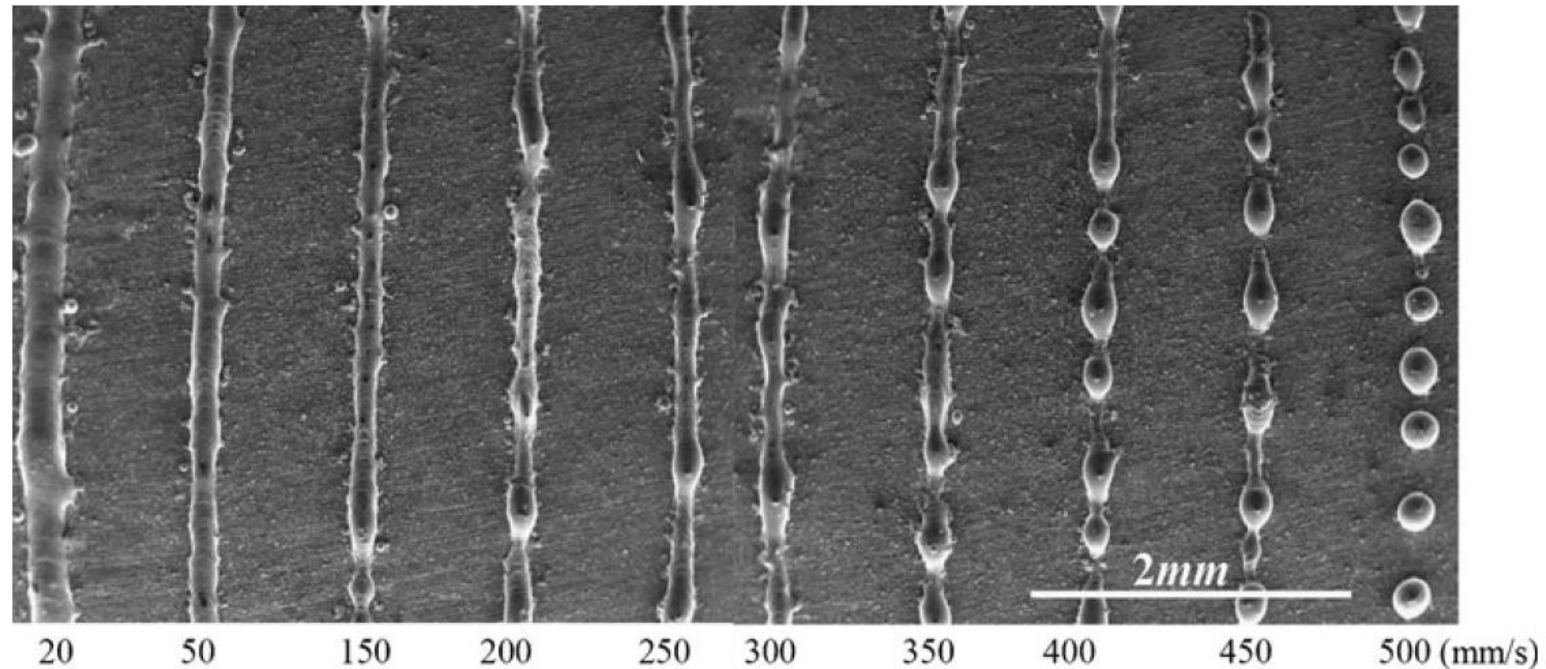
Effet « balling »

Int J Adv Manuf Technol (2012) 59:1025–1035
DOI 10.1007/s00170-011-3566-1

ORIGINAL ARTICLE

Balling behavior of stainless steel and nickel powder during selective laser melting process

Ruidi Li · Jinhui Liu · Yusheng Shi · Li Wang ·
Wei Jiang



Acta Materialia 114 (2016) 33–42

Contents lists available at ScienceDirect

Acta Materialia

journal homepage: www.elsevier.com/locate/actamat

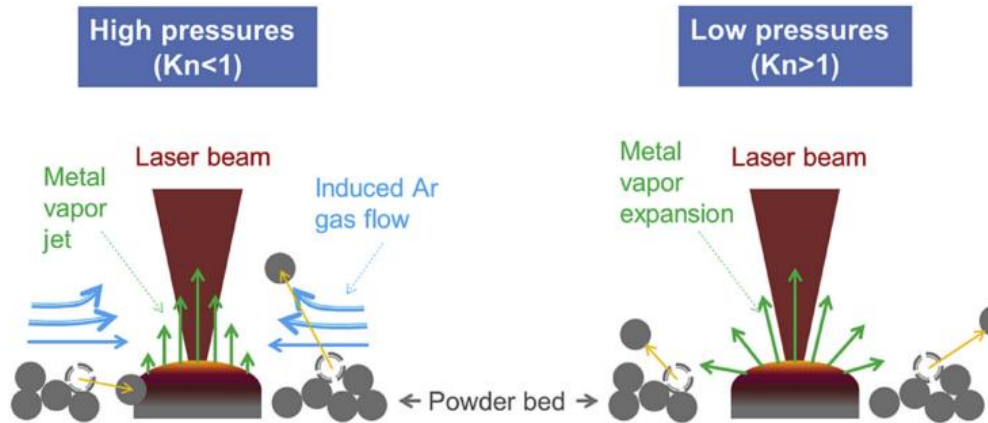
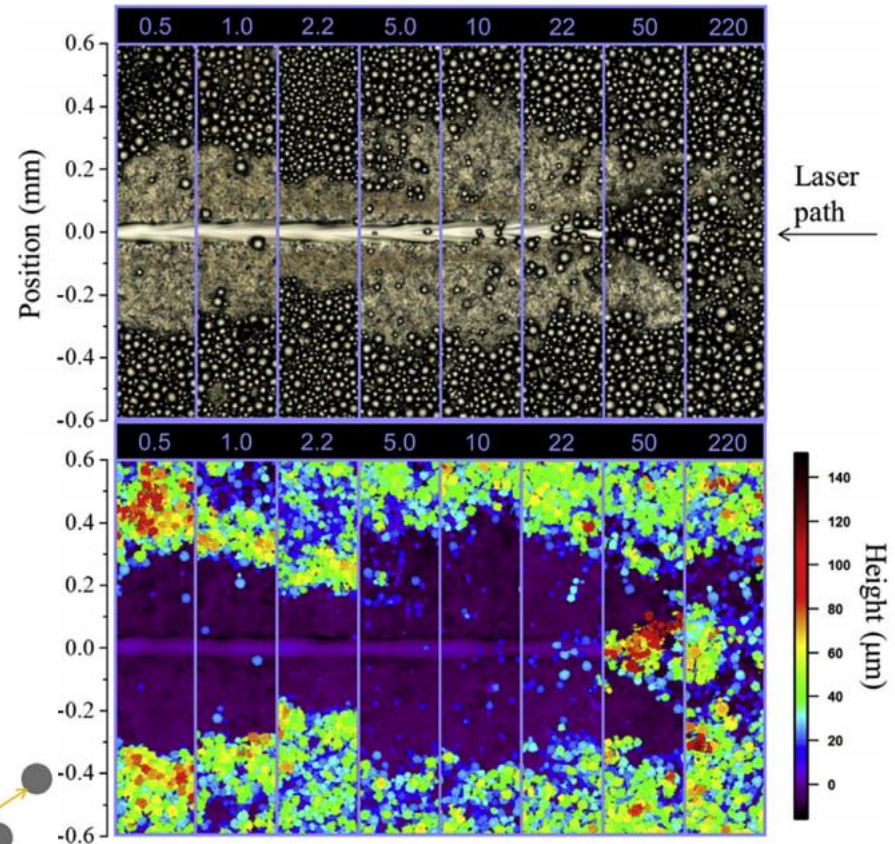


Full length article

Denudation of metal powder layers in laser powder bed fusion processes

Manyalibo J. Matthews*, Gabe Guss, Saad A. Khairallah, Alexander M. Rubenchik, Philip J. Depond, Wayne E. King

Lawrence Livermore National Laboratory, 7000 East Avenue, Livermore, CA 94550, USA



Vidéo : Denudation

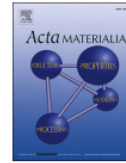


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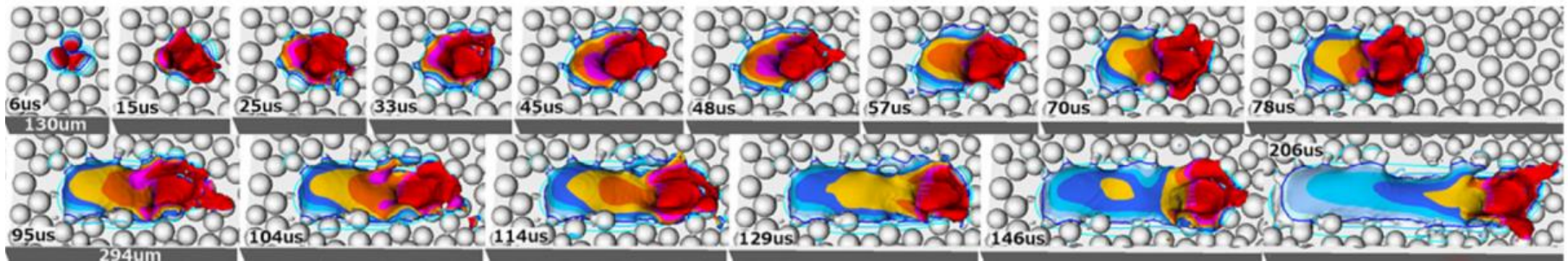
Full length article

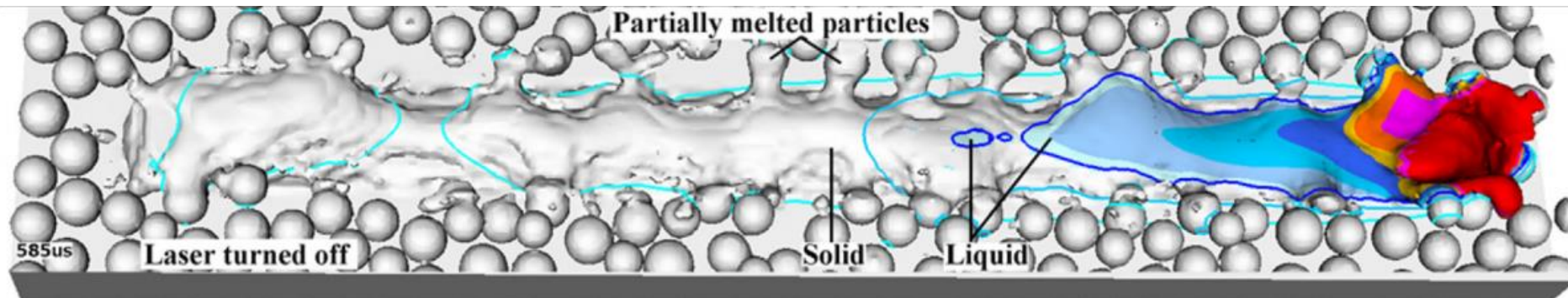
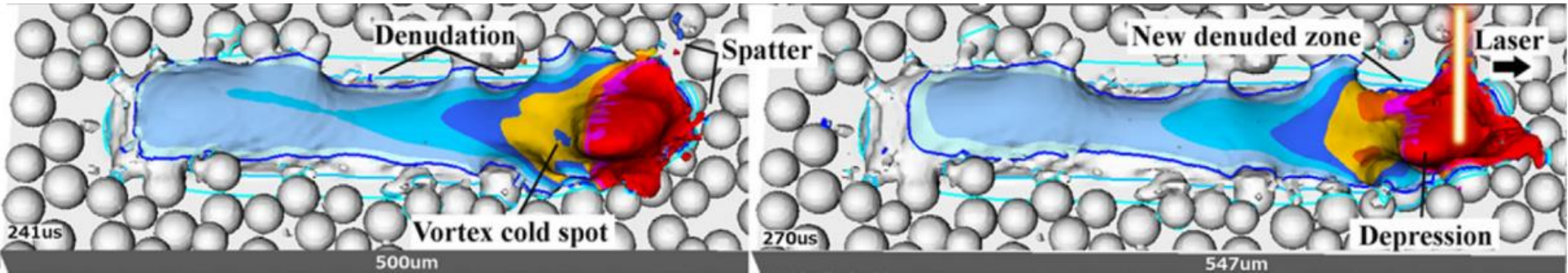
Laser powder-bed fusion additive manufacturing: Physics of complex melt flow and formation mechanisms of pores, spatter, and denudation zones

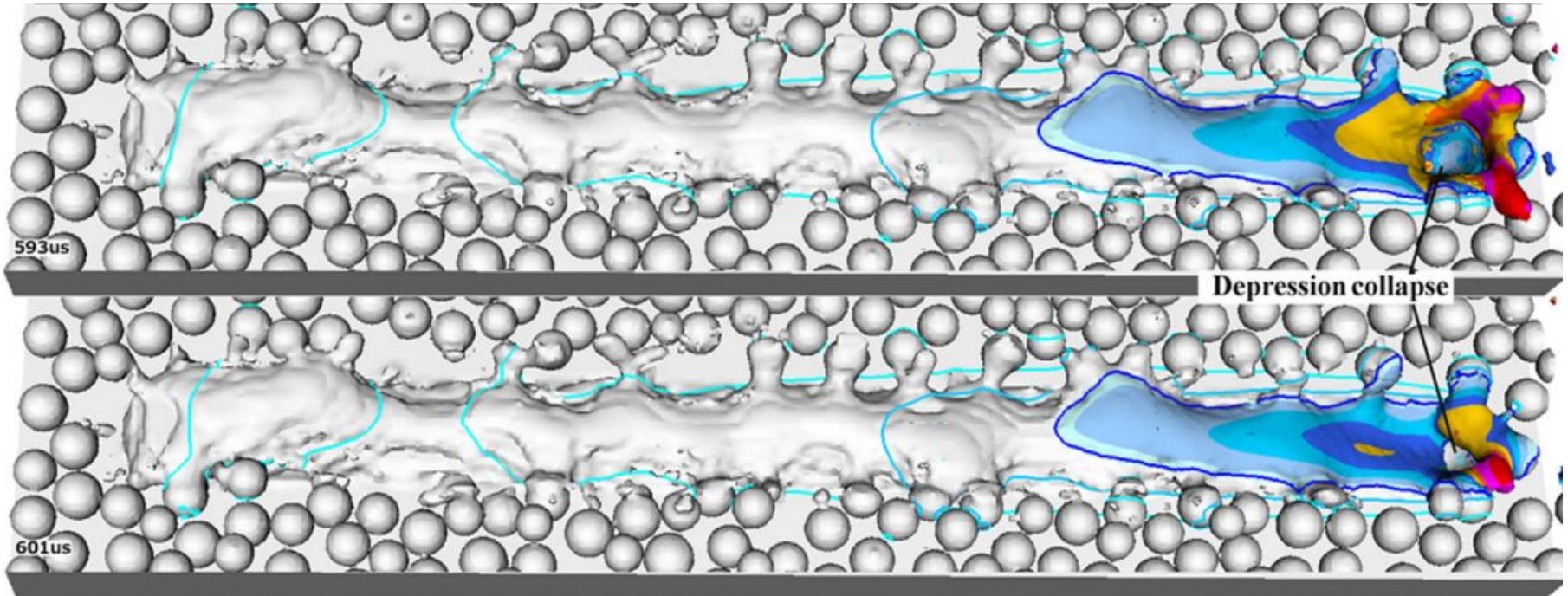


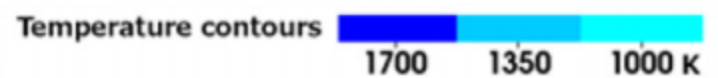
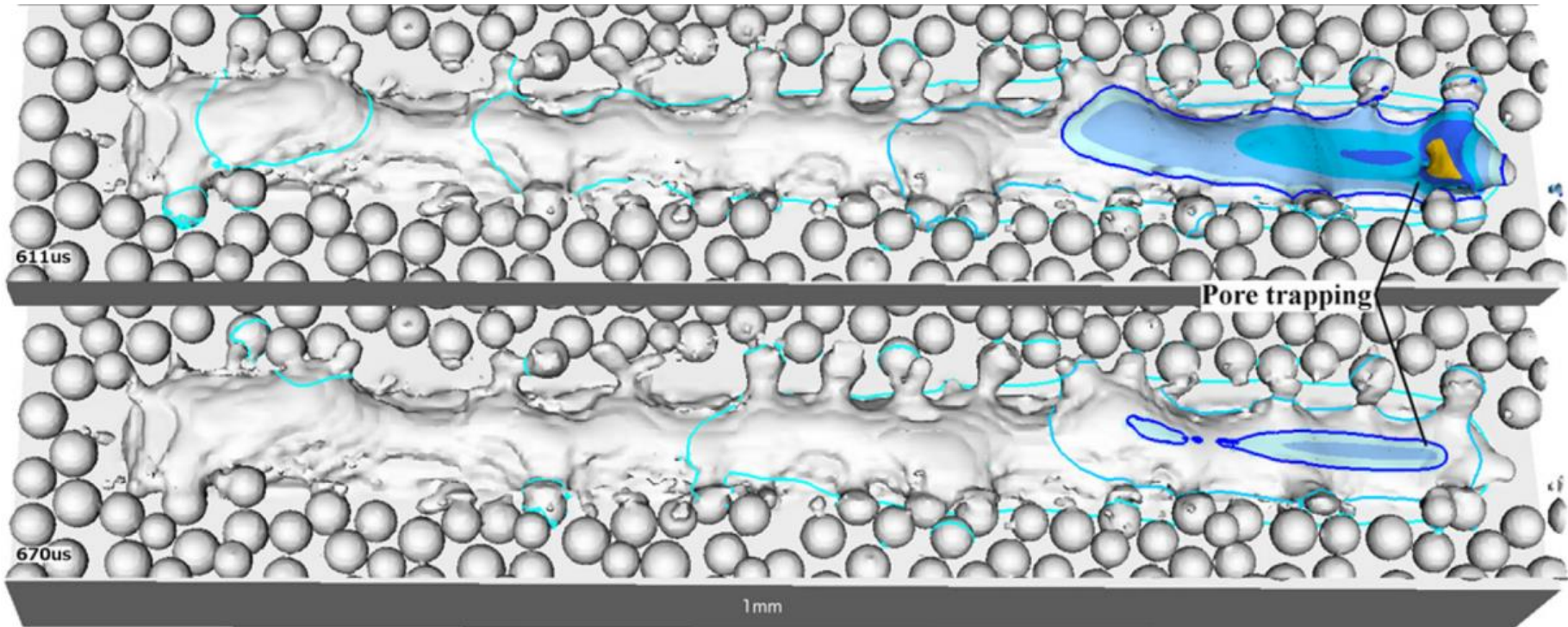
Saad A. Khairallah*, Andrew T. Anderson, Alexander Rubenchik, Wayne E. King

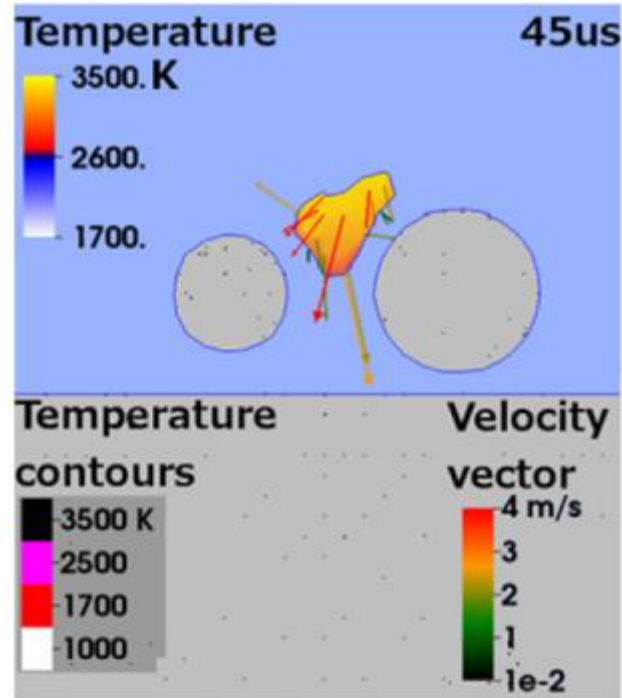
Lawrence Livermore National Laboratory, 7000 East Ave. Livermore, CA 94550, USA

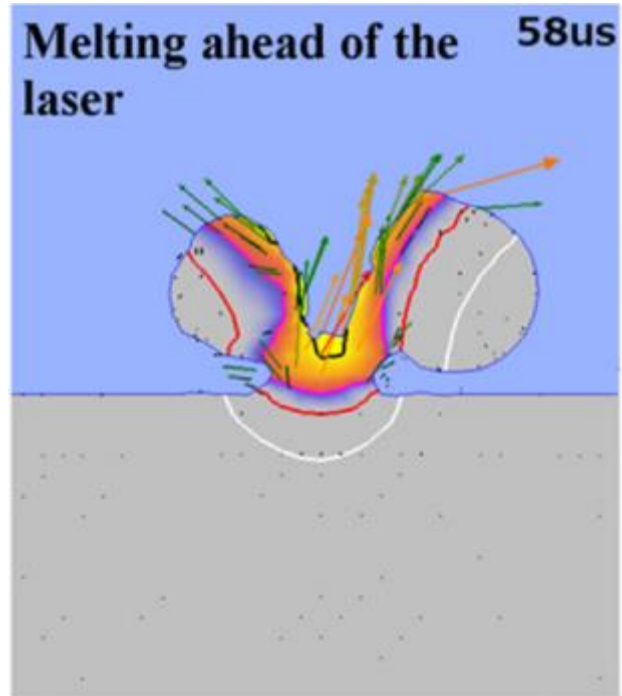


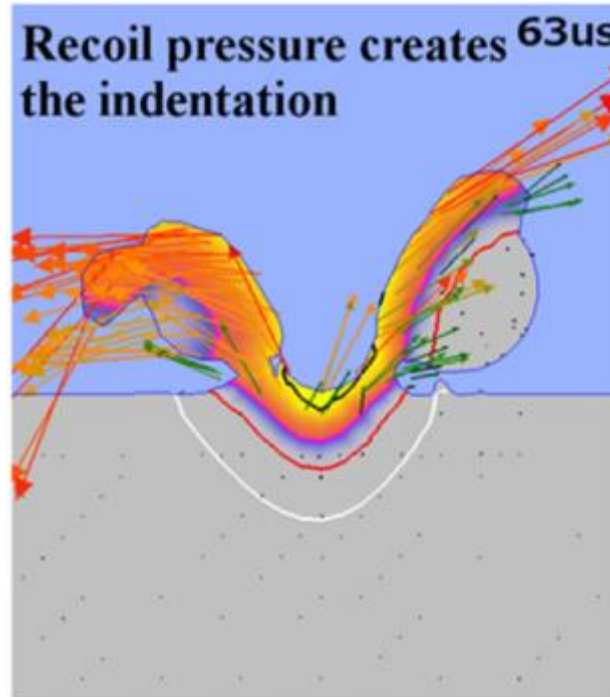


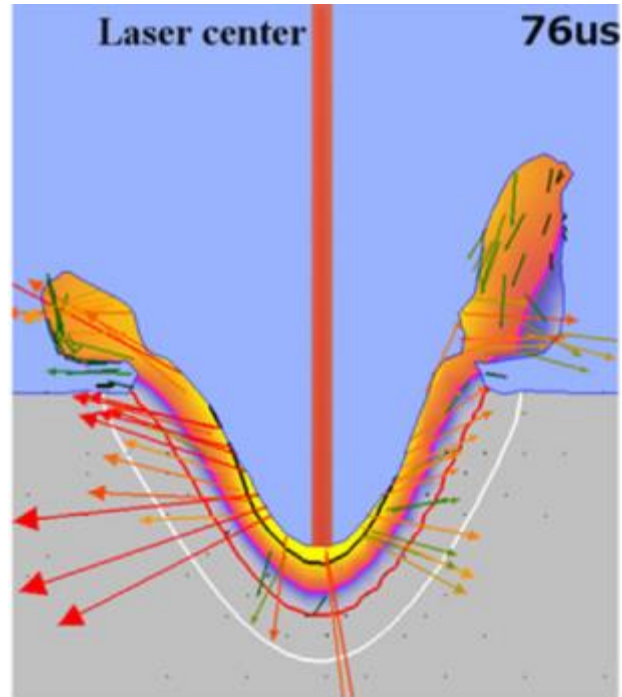


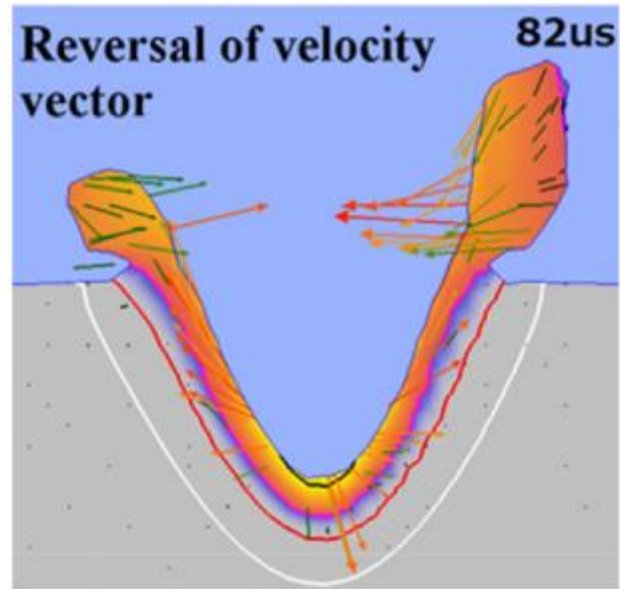


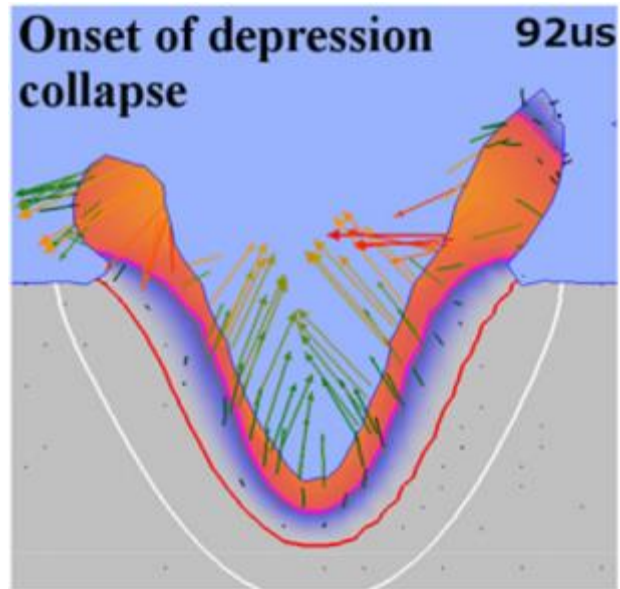


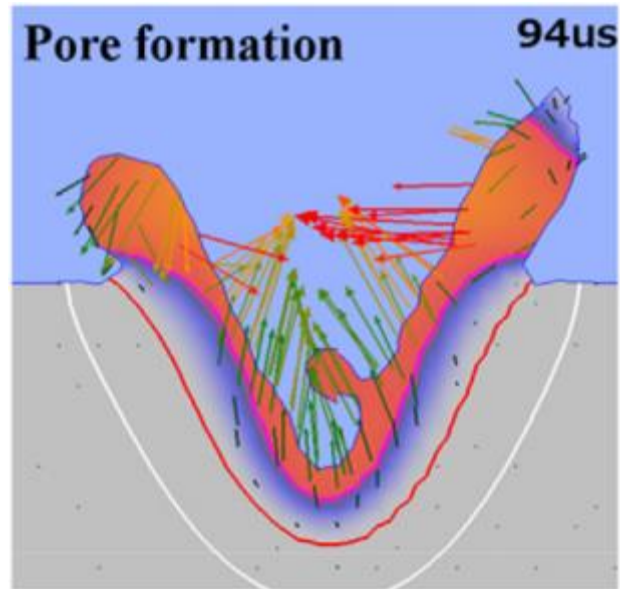


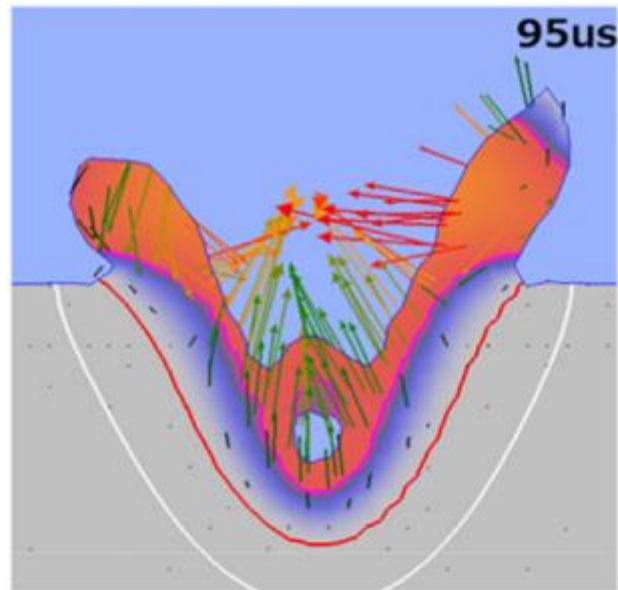






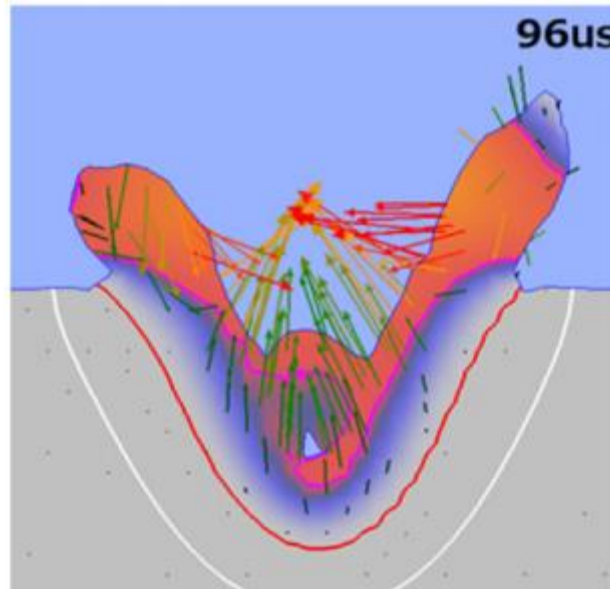


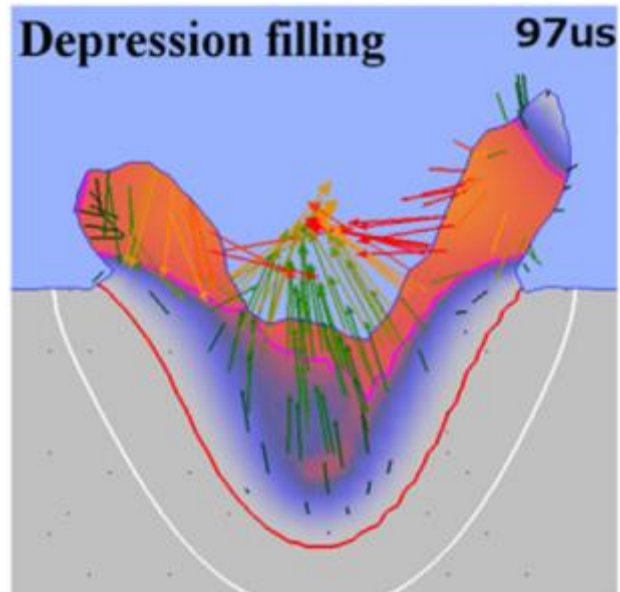


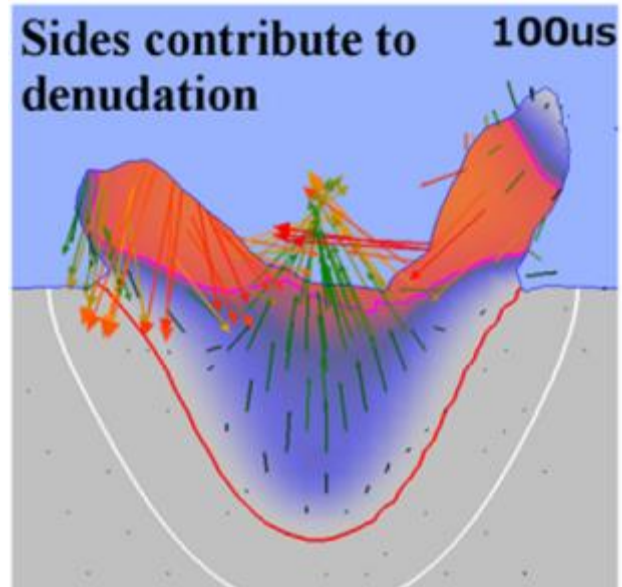


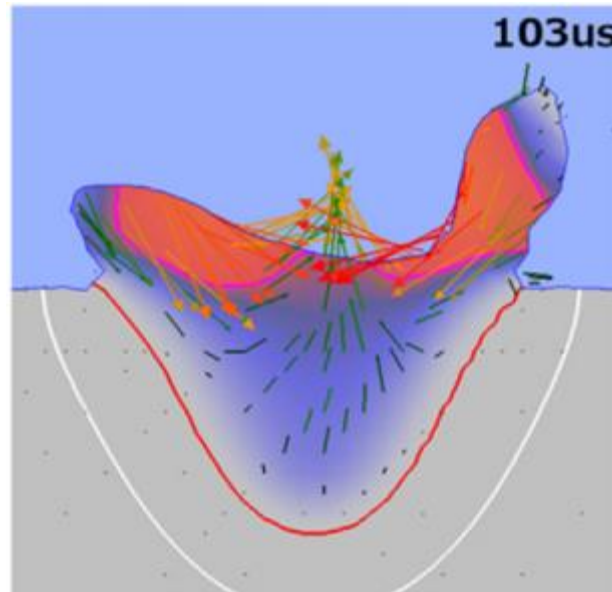
Formation de porosités :

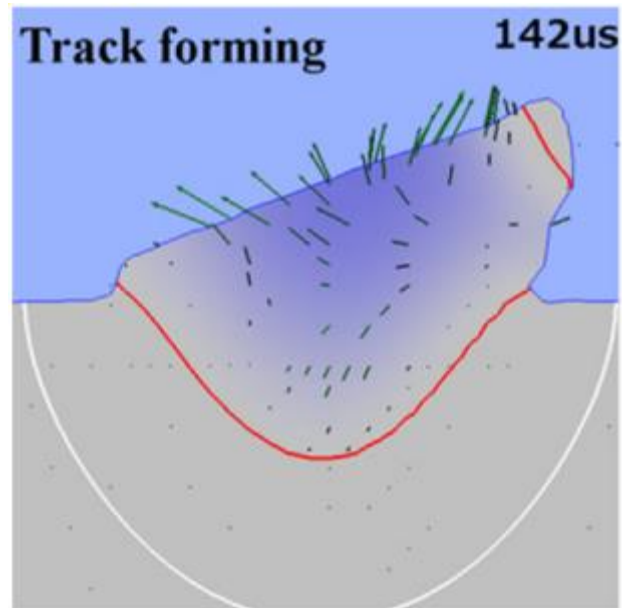
- Dynamique du bain et/ou génération de gaz (ex : Aluminium)
- Viscosité du bain (matériau)
- Dimensions du bain, vitesse du laser

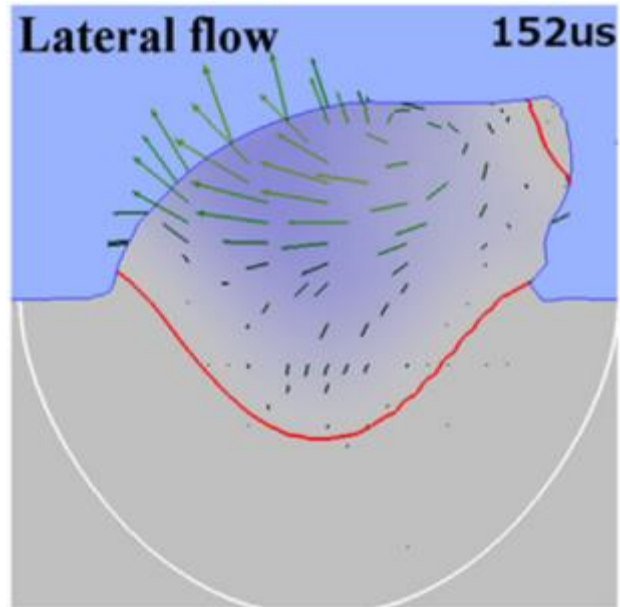


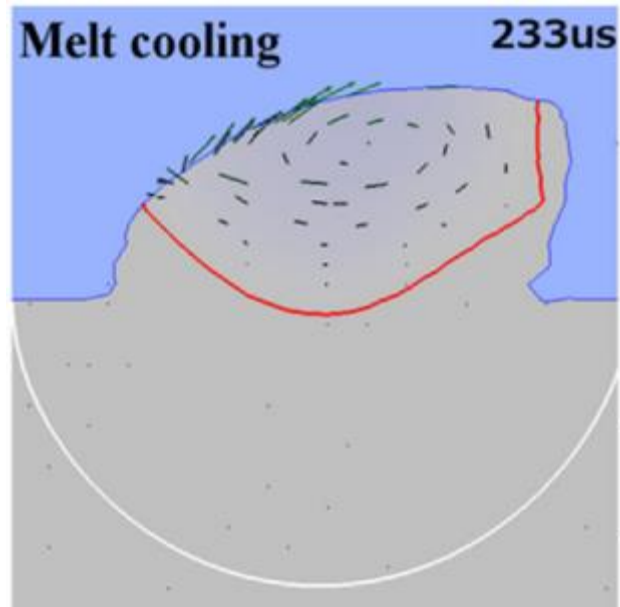


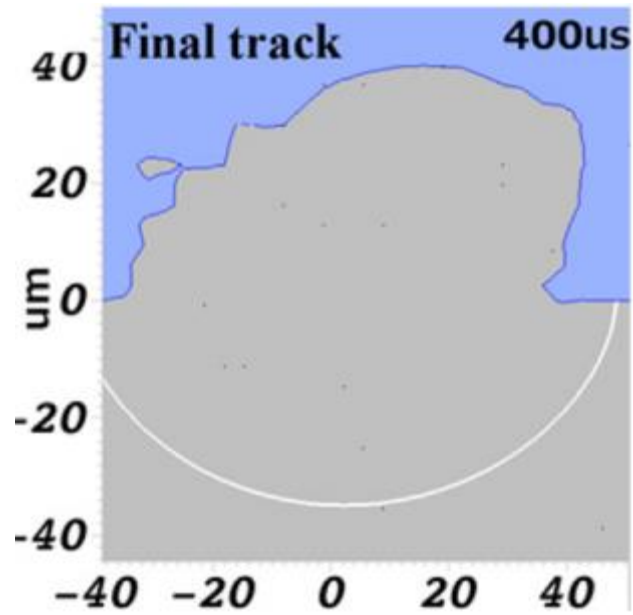












Maîtriser la dynamique du bain



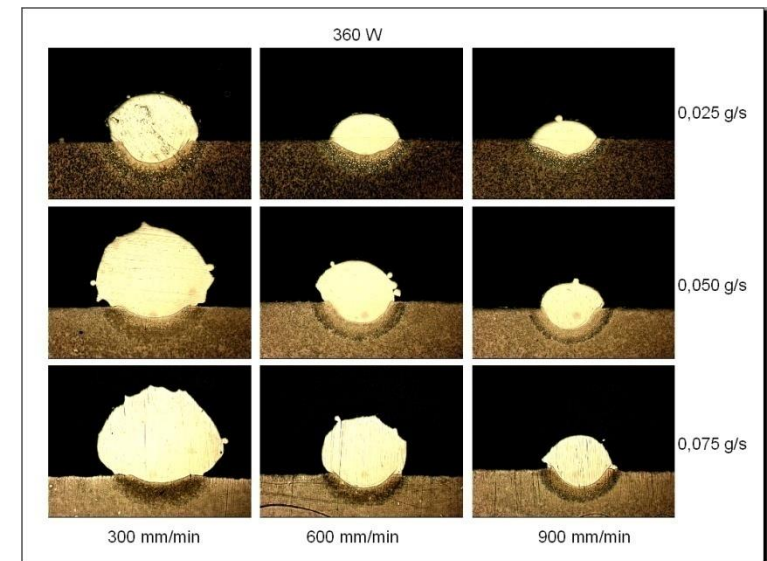
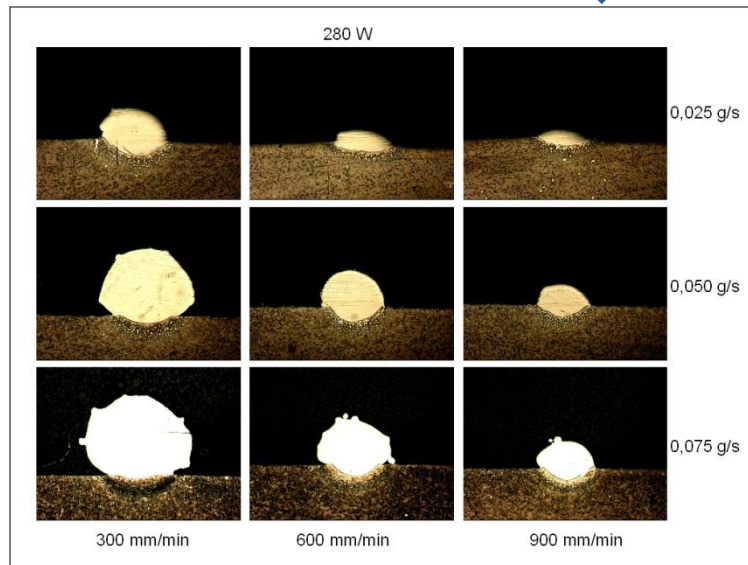
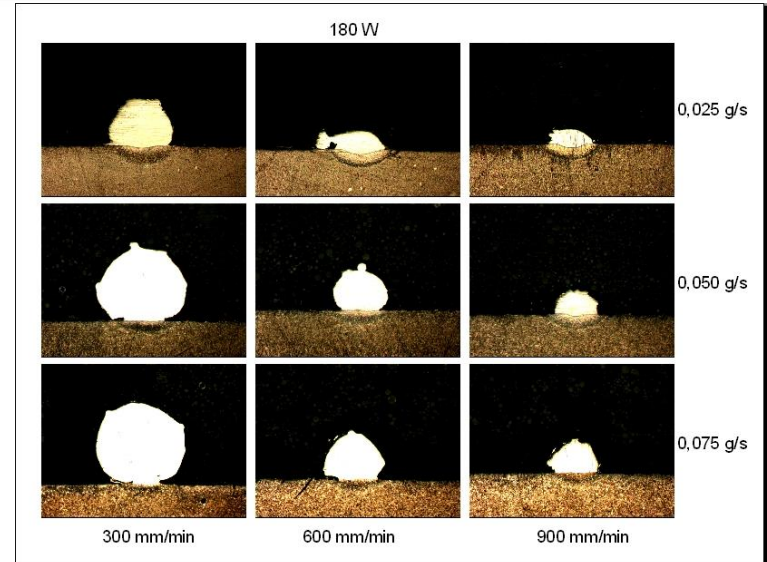
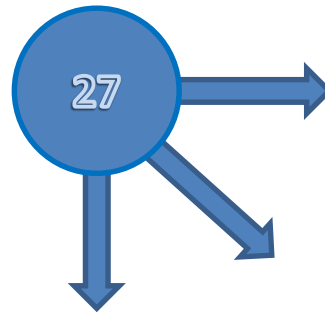
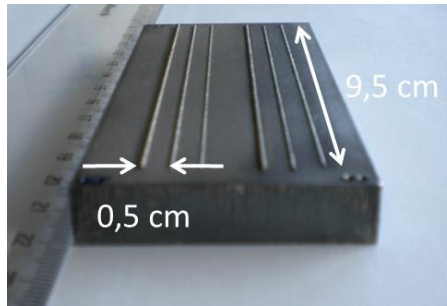
Réaliser un mur

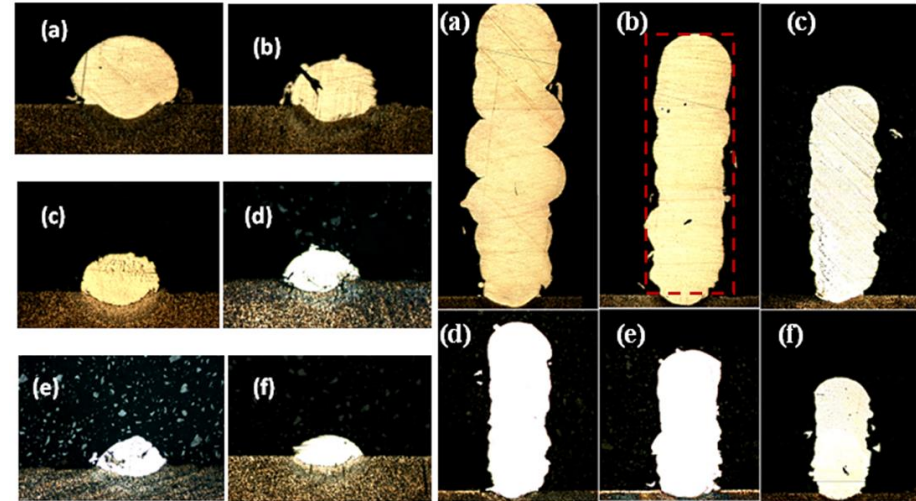
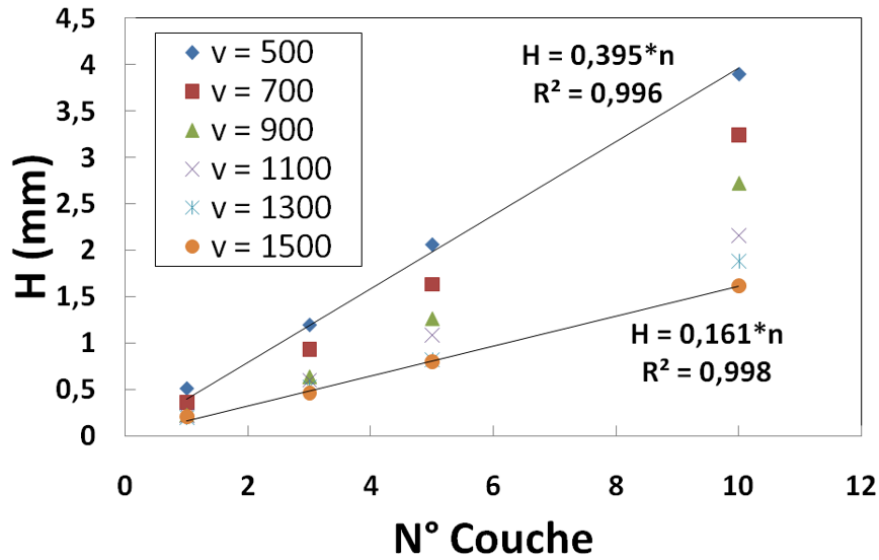
3 paramètres avec 3 niveaux

Puissance laser : P

Débit de poudre : Q_m

Vitesse relative : V





Relation linéaire entre la hauteur du mur et le nombre de couches



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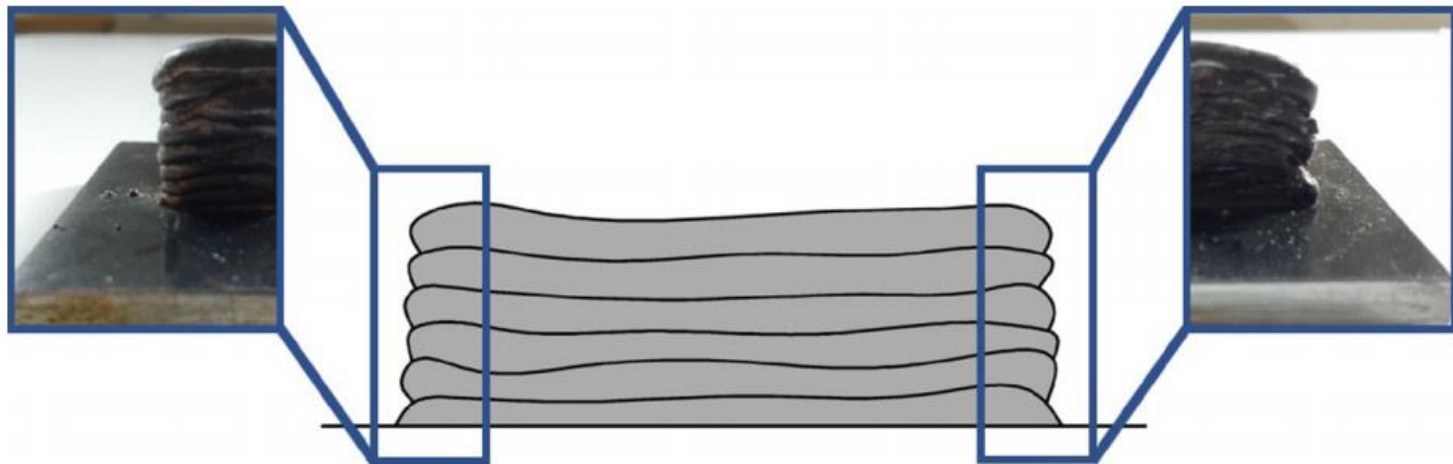
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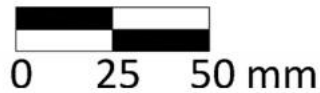
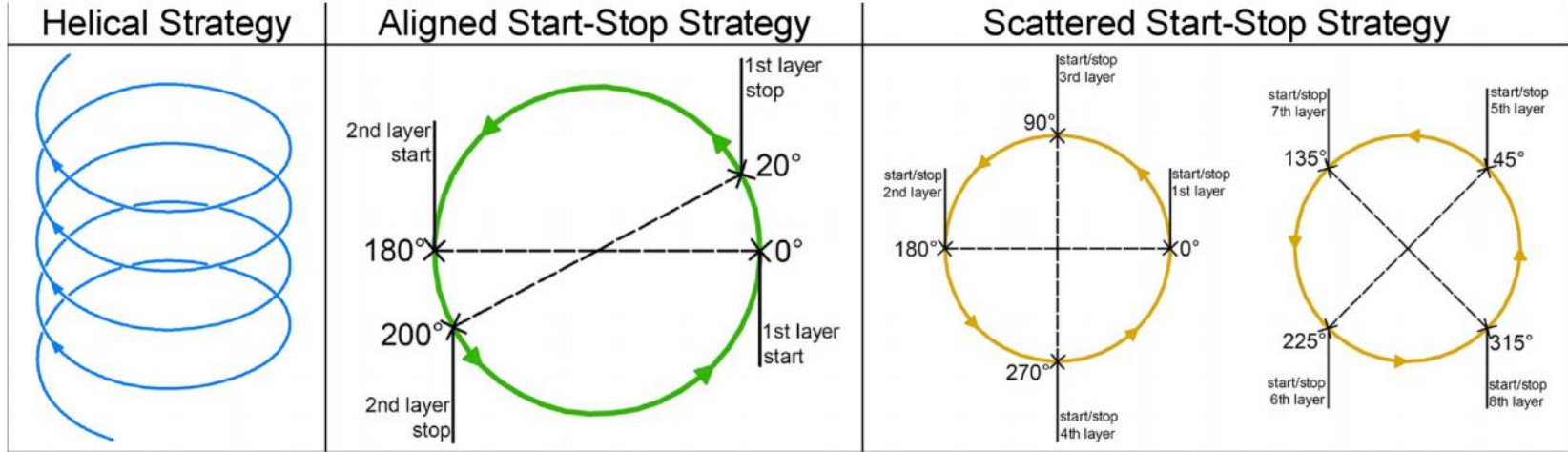
Feature based three axes computer aided manufacturing software for wire arc additive manufacturing dedicated to thin walled components



Giuseppe Venturini*, Filippo Montevercchi, Francesco Bandini, Antonio Scippa, Gianni Campatelli

Department of Industrial Engineering, University of Firenze, Via di Santa Marta 3, Firenze, 50139, Italy





Maîtriser la distance buse – pièce et la géométrie du bain

Réaliser une structure pleine



Additive Manufacturing 14 (2017) 39–48



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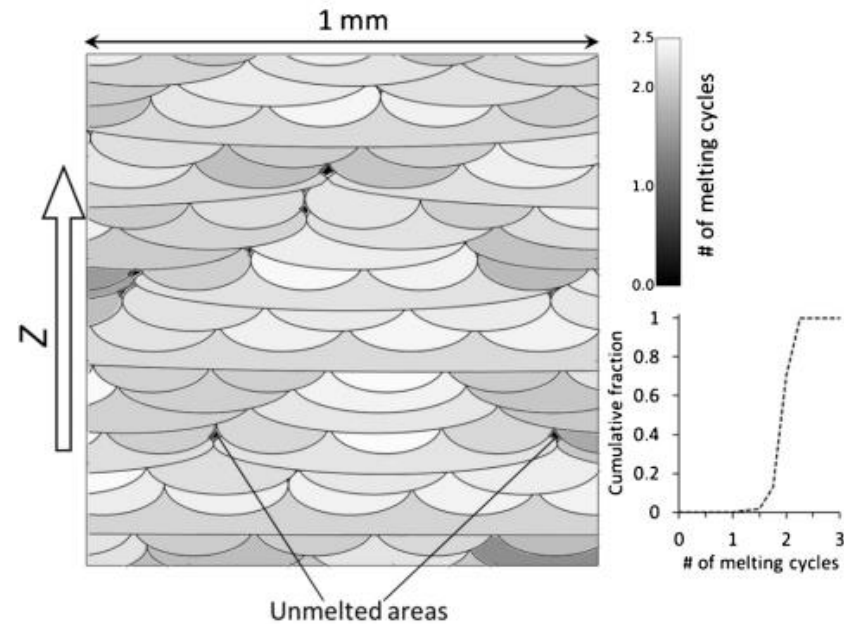
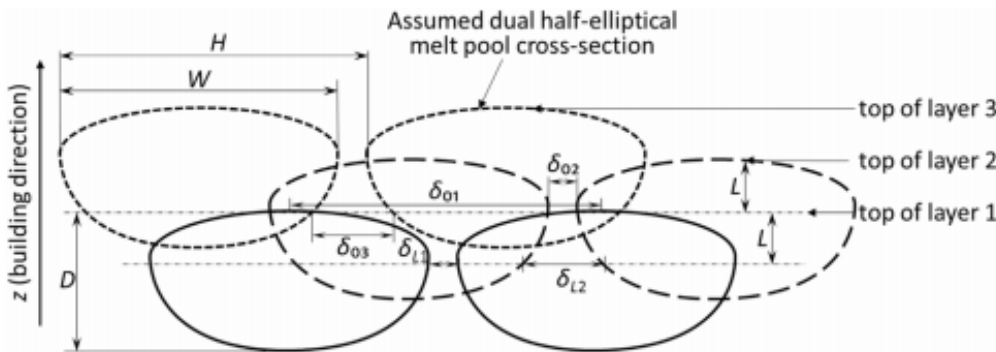
Full Length Article

Prediction of lack-of-fusion porosity for powder bed fusion[☆]

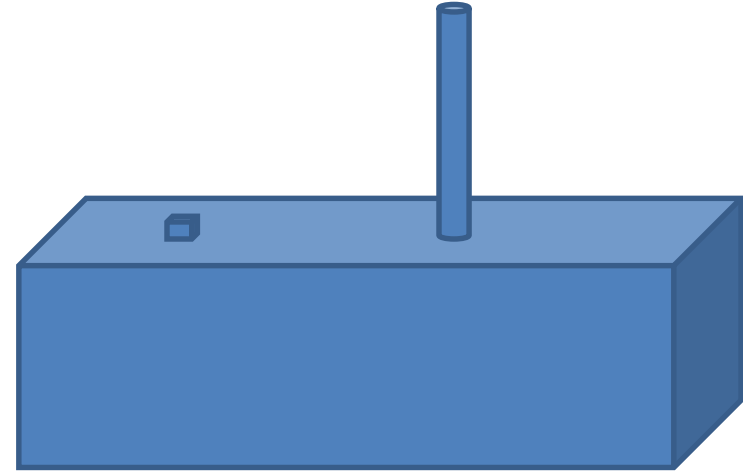
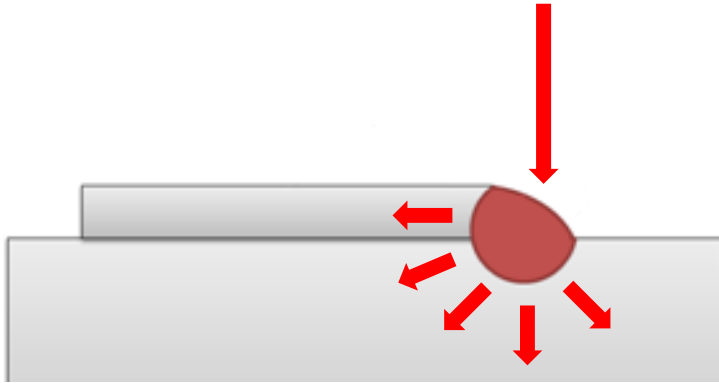
Ming Tang^a, P. Chris Pistorius^{a,*}, Jack L. Beuth^b

^a Department of Materials Science and Engineering, Carnegie Mellon University, 5000 Forbes Avenue, Pittsburgh, PA, 15213, USA

^b Department of Mechanical Engineering, Carnegie Mellon University, 5000 Forbes Avenue, Pittsburgh, PA, 15213, USA



Réaliser une pièce



Les conditions thermiques changent les paramètres doivent s'adapter

Simulations EF trop lourdes

Simulations analytiques trop grossières



Suivi in-situ par CND

Additive Manufacturing 12 (2016) 1–15

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Understanding the effect of laser scan strategy on residual stress in selective laser melting through thermo-mechanical simulation

L. Parry, I.A. Ashcroft*, R.D. Wildman

University of Nottingham, Nottingham, NG7 2RD, UK

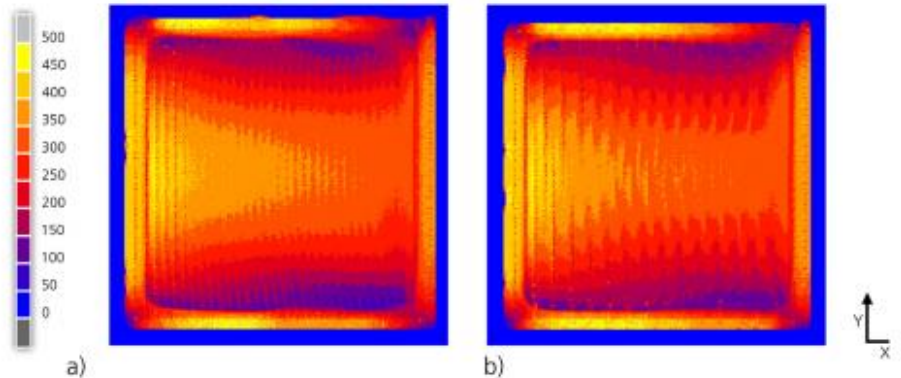
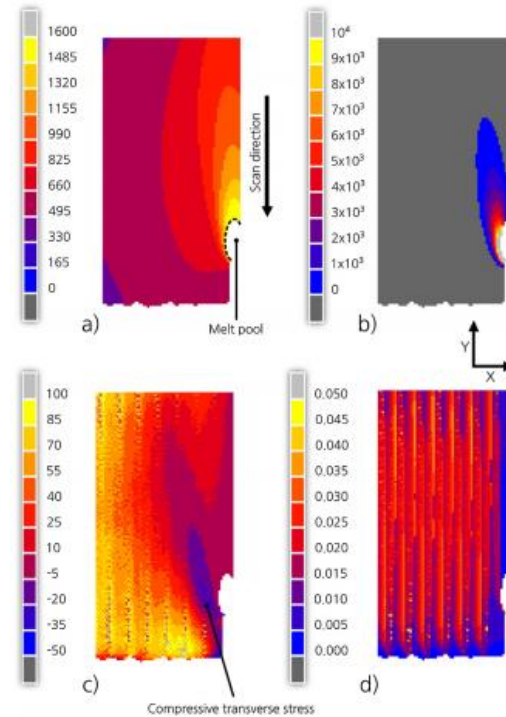
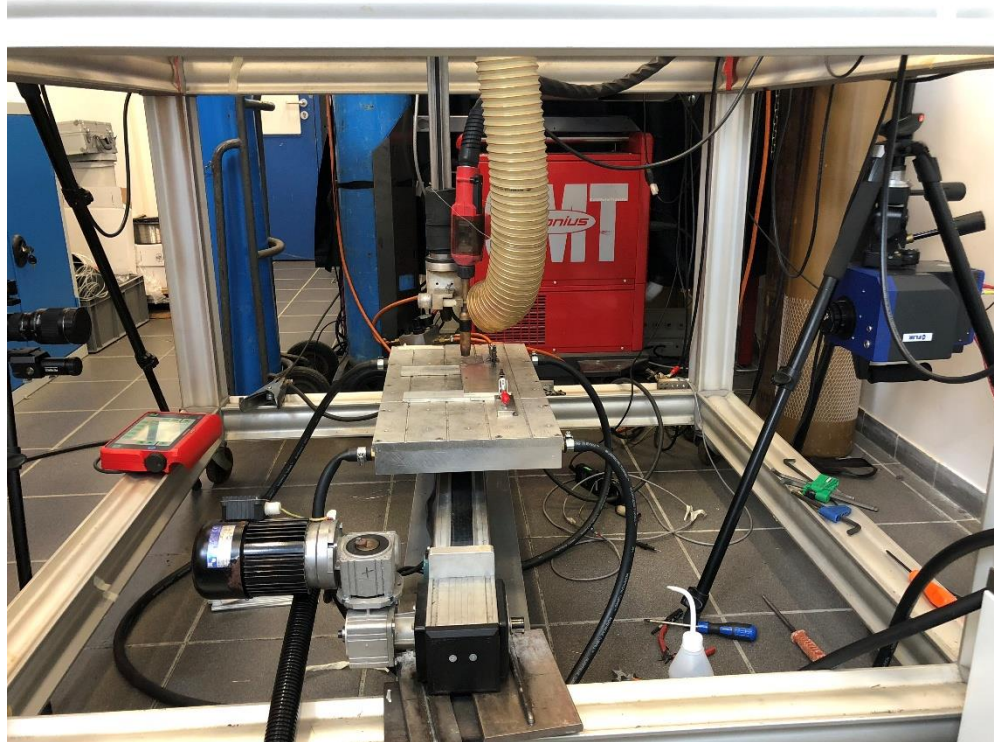


Fig. 15. Profiles views of von Mises stress distribution for 3 mm × 3 mm test case when using a) unidirectional, and b) alternating scan strategies

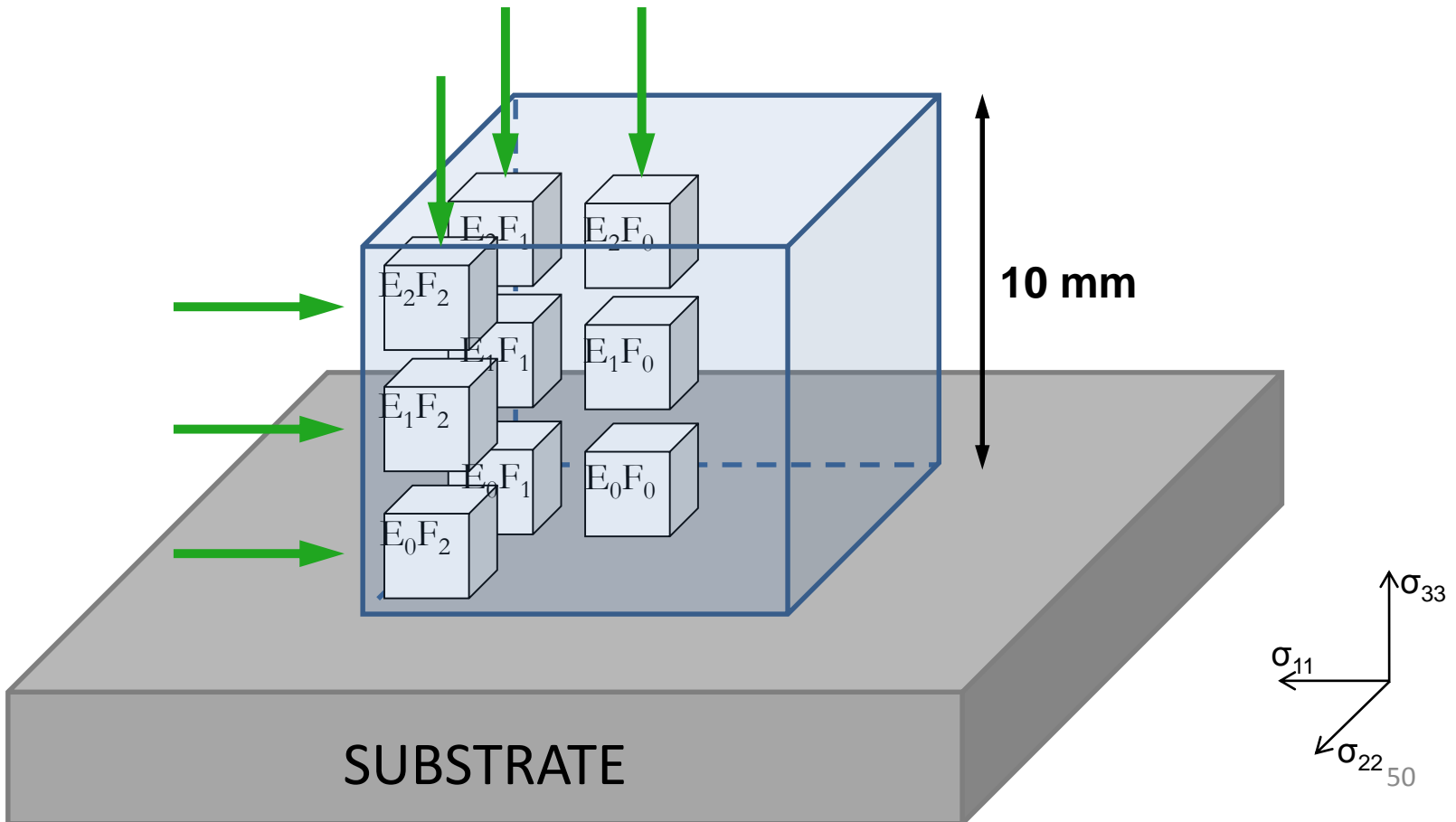


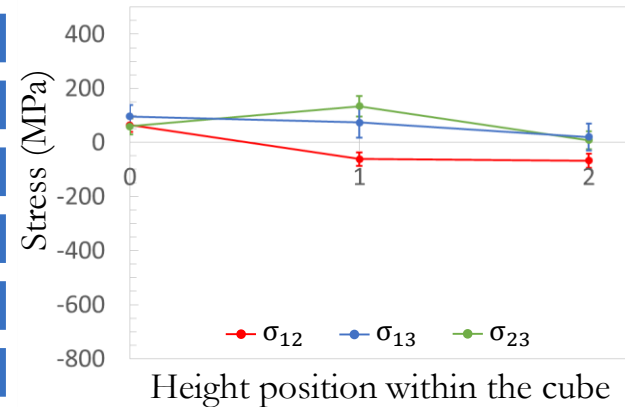
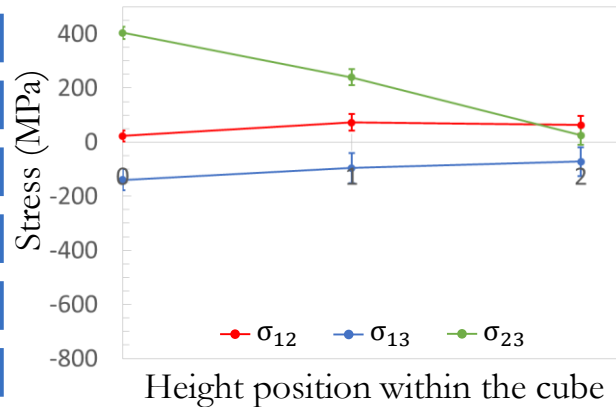
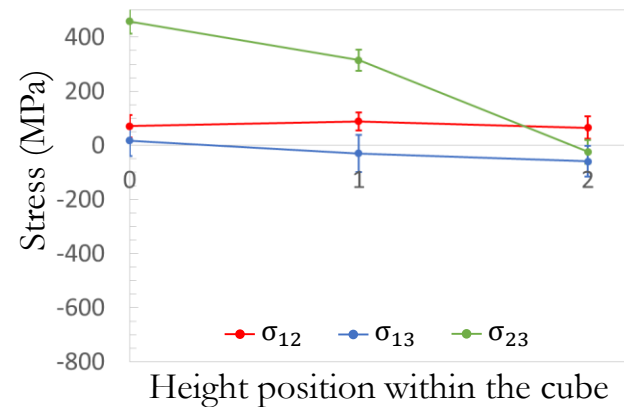
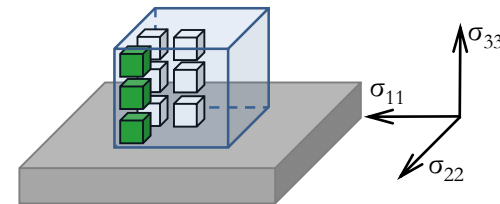
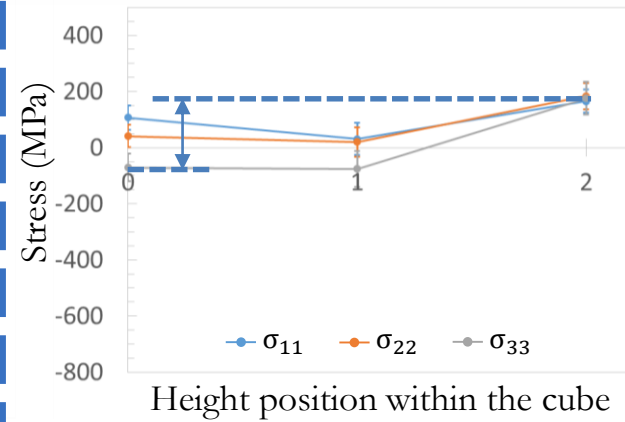
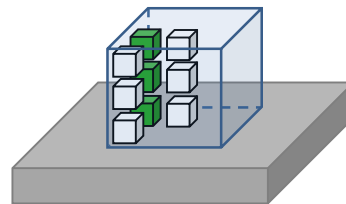
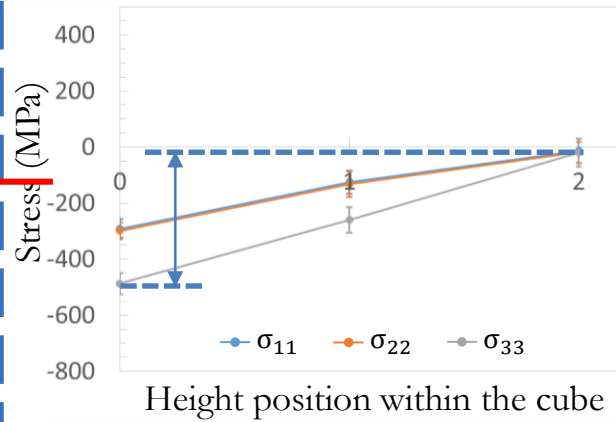
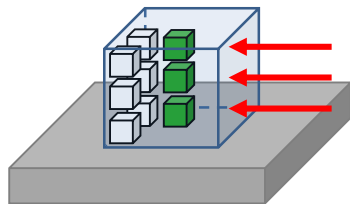
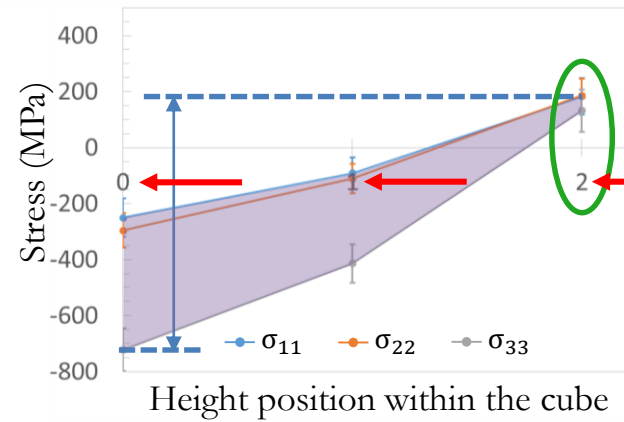


à gauche la camera haute vitesse et a droite la camera infra rouge

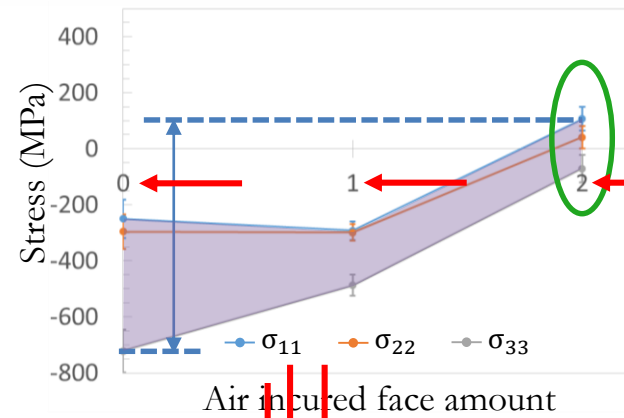


- Analysis of **9** volumes (strain gage) of **2×2×2 mm³** (200 μm from edges) distributed over the cube:
 - **Full stress tensor analysis at each gage position**:
 - ▶ Along each **column**: emphasis made on **thermal background (E₀ or E₁ or E₂)**
 - ▶ On each **level**: focus on **heat treatment** induced by the amount of **close surface (F₀ or F₁ or F₂)**

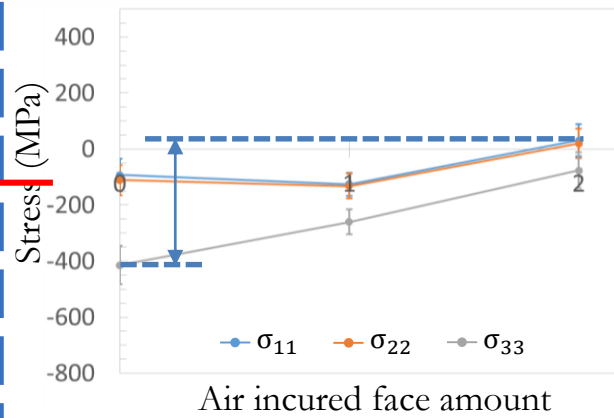
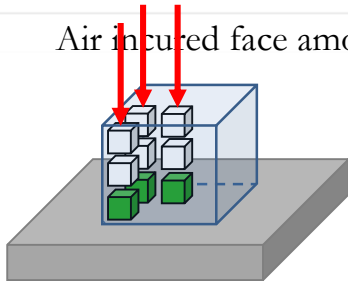




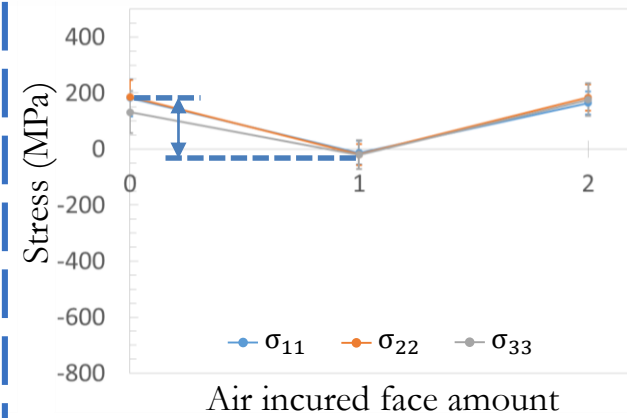
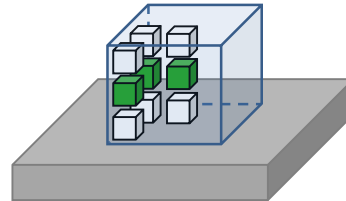
- ▶ Reduction of residual stress gradient magnitude with building height
- ▶ **Homogeneous** and **lowered values** close to upper surface
- ▶ The **larger** quenching surface, the **smaller** residual stress **gradient magnitude**



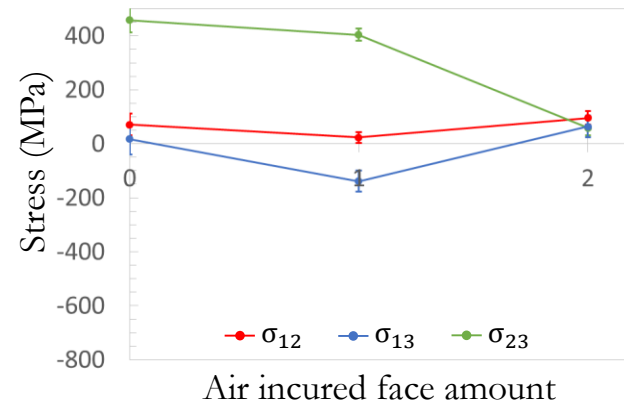
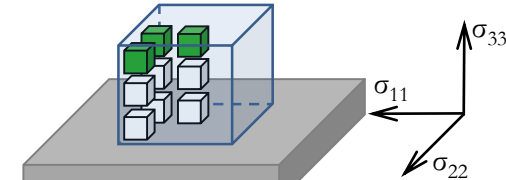
Air incured face amount



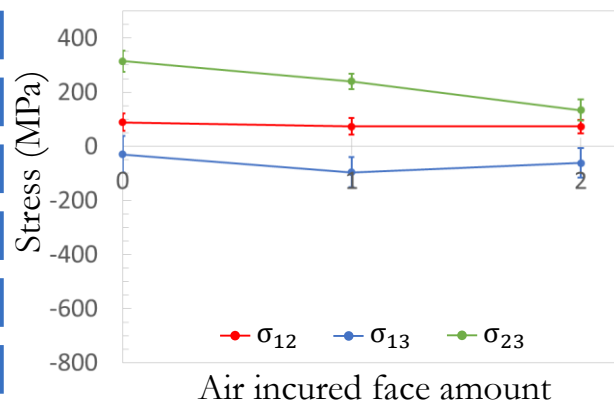
Air incured face amount



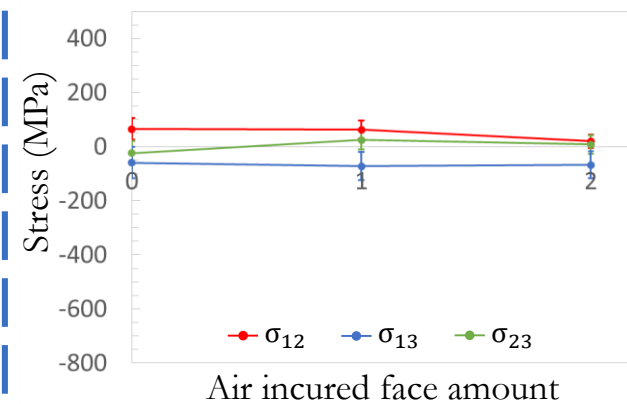
Air incured face amount



Air incured face amount



Air incured face amount



Air incured face amount

- ▶ Reduction of residual stress gradient magnitude with quenching face amount
- ▶ **Homogeneous and lowered values close to corners**
- ▶ The **higher**, the **smaller** residual stress gradient magnitude

Maîtriser les phénomènes thermiques

Les CND doivent pouvoir contribuer à éviter les principaux problèmes rencontrés en fabrication additive :

Vérifier la bonne formation du cordon

Eviter la formation de porosités

Maîtriser la dynamique du bain

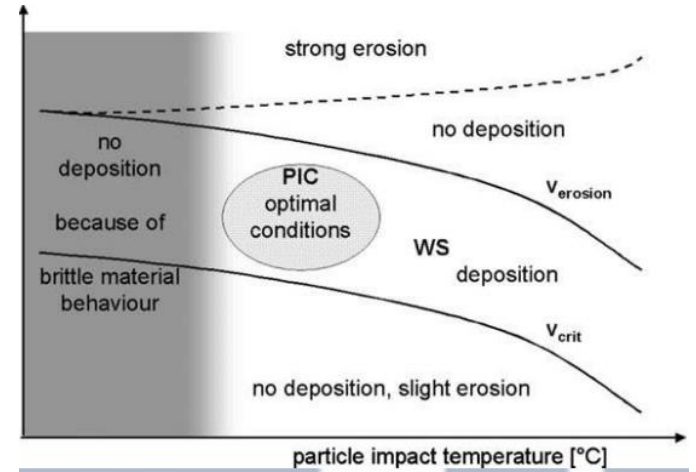
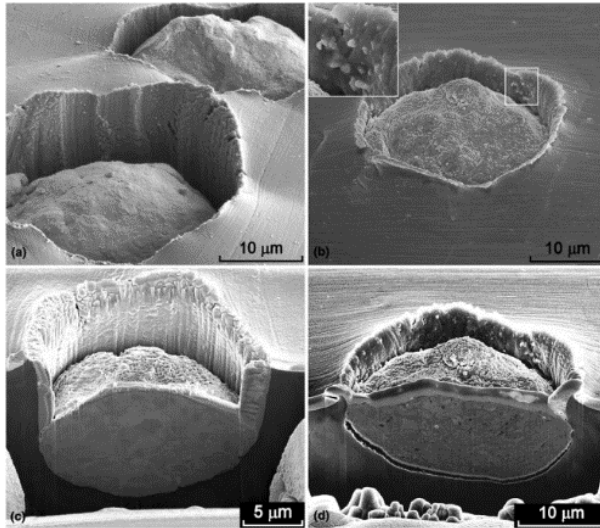
Assurer la stabilité lors de la fabrication de pièces hautes

Maîtriser la distance buse – pièce et la géométrie du bain

Limiter la présence des contraintes résiduelles

Maîtriser les phénomènes thermiques

Un procédé de fabrication additive sans fusion : Projection à froid (cold spray)



T. Schmidt et al. / Acta Materialia 54 (2006) 729–742

